

Indian Institute of Science, Bangalore

ME 243: Endsemester Exam

Date: 1/12/25.

Duration: 9.00 a.m.–12.00 noon

Maximum Marks: 100

Instructions:

You may directly use the formulae at the back.

1. If (20)

$$[\mathbf{T}\mathbf{u}, \mathbf{T}\mathbf{v}, \mathbf{w}] = [\mathbf{u}, \mathbf{v}, \mathbf{T}^T\mathbf{w}] \quad \forall \mathbf{u}, \mathbf{v}, \mathbf{w} \in V,$$

and if $\mathbf{T} \neq \mathbf{0}$, then find the most general form of \mathbf{T} . Justify each step.

2. A small rigid body of mass M slides along a frictionless circular wire of radius (25)

R which rotates with angular velocity $\omega \mathbf{e}_y$ (which is equal to $\boldsymbol{\Omega}$) and angular acceleration $\dot{\omega} \mathbf{e}_y$ (which is equal to $\dot{\boldsymbol{\Omega}}$) as shown in Fig. 1. The gravitational body force with respect to a *fixed* frame of reference is $-g \mathbf{e}_y$. Assuming that the body force is a constant over the material volume occupied by the body (so that $\int_V \rho \mathbf{b} dV = M \mathbf{b}$), and starting from any of the balance laws of your choice for a material volume, *derive* the governing equation for the angular position $\theta(t)$ of the center of mass of the body. The initial conditions are given by $\theta(0) = \theta_0$ and $\dot{\theta}(0) = \alpha$. Multiply your governing equation by $\dot{\theta}$ and integrate once, with the integration constant determined using the initial conditions.

3. A circular hole of radius b in an unbounded domain is subjected to a shear (25)

traction $t_\theta = s_0$. Assume that the deformation is independent of Z . Further assume $r = \alpha R$, $z = Z$, and assume a suitable mapping for θ in terms of an unknown function. The material is incompressible, and the constitutive equation is given by $\boldsymbol{\tau} = -p \mathbf{I} + \mu \mathbf{B}$.

- (a) Find the constant α , and the governing differential equation for your unknown function and any other unknown field.
- (b) State the boundary conditions for your unknown function and the other unknown field.
- (c) Solve for your unknown function and any other unknown field.

4. With ψ denoting the free energy, and $\boldsymbol{\tau}$ denoting the Cauchy stress tensor, (30)
the constitutive relations for a homogeneous, isotropic solid are given by

$$\begin{aligned} \psi &= \hat{\psi}(\mathbf{F}, \mathbf{L}), \\ \boldsymbol{\tau} &= \hat{\boldsymbol{\tau}}(\mathbf{F}, \mathbf{L}), \end{aligned}$$

where $\boldsymbol{\tau}$ is a continuous function of \mathbf{L} .

- (a) If $\mathbf{S} \in \text{Sym}$, $\mathbf{T} \in \text{Lin}$ and $\mathbf{T}_s = (\mathbf{T} + \mathbf{T}^T)/2$, then show that $\mathbf{S} : \mathbf{T} = \mathbf{S} : \mathbf{T}_s$.
- (b) Starting from $\dot{\mathbf{F}} = \mathbf{L}\mathbf{F}$, and with $\mathbf{B} = \mathbf{F}\mathbf{F}^T$, derive an expression for $\dot{\mathbf{B}}$ in terms of \mathbf{F} and \mathbf{L} . Similarly, derive an expression for \mathbf{D} as a function of $\dot{\mathbf{F}}$ and \mathbf{F} .
- (c) Using $\mathbf{F}^* = \mathbf{Q}\mathbf{F}$, derive an expression for \mathbf{L}^* in terms of \mathbf{L} .
- (d) Successively applying material frame-indifference and the condition for isotropy, carry out appropriate reductions in the form for $\hat{\psi}$. (e.g., dependence on \mathbf{F} reduces to a dependence on \mathbf{U} or \mathbf{V} .) Provide detailed arguments for each such reduction. If you are using any theorem covered in class, cite the theorem (Hint: You can express functions of \mathbf{U} and \mathbf{V} as functions of \mathbf{C} and \mathbf{B} , respectively, to simplify your analysis).
- (e) Using the isothermal version of the Clausius-Duhem inequality given by

$$\dot{\psi} - \frac{1}{\rho} \boldsymbol{\tau} : \mathbf{L} \leq 0,$$

find the equalities and inequalities (necessary and sufficient conditions) that result. In the proof for this part, *do not* attempt to construct an admissible thermodynamic process; assume that such a process can be constructed for arbitrary values of your kinematical variables. *Justify* all steps.

Some relevant formulae

$$\begin{aligned} \frac{\partial I_1}{\partial \mathbf{T}} &= \mathbf{I}, \\ \frac{\partial I_2}{\partial \mathbf{T}} &= (\text{tr } \mathbf{T})\mathbf{I} - \mathbf{T}^T, \\ \frac{\partial I_3}{\partial \mathbf{T}} &= \text{cof } \mathbf{T}, \\ \mathbf{b} &= \mathbf{Q}^T (\mathbf{b}^* - \ddot{\mathbf{c}}) - \dot{\boldsymbol{\Omega}} \times \mathbf{x} - \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{x}) - 2\boldsymbol{\Omega} \times \mathbf{v}, \\ Q_{ij} &= \mathbf{e}_i^* \cdot \mathbf{e}_j, \\ \mathbf{R} : (\mathbf{S}\mathbf{T}) &= (\mathbf{S}^T \mathbf{R}) : \mathbf{T} = (\mathbf{R}\mathbf{T}^T) : \mathbf{S} = (\mathbf{T}\mathbf{R}^T) : \mathbf{S}^T, \\ F_{iJ} &= \frac{h_i}{h_J} \frac{\partial \hat{\chi}_i}{\partial \eta_J}, \quad \text{no sum on } i, J, \quad h_i \equiv (1, r, 1), \quad h_J \equiv (1, R, 1). \end{aligned}$$

If $\boldsymbol{\tau}$ is symmetric tensor-valued field, then the components of $\boldsymbol{\nabla}_x \cdot \boldsymbol{\tau}$ with respect to a cylindrical coordinate system are

$$\begin{aligned} (\boldsymbol{\nabla} \cdot \boldsymbol{\tau})_r &= \frac{\partial \tau_{rr}}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\theta}}{\partial \theta} + \frac{\partial \tau_{rz}}{\partial z} + \frac{\tau_{rr} - \tau_{\theta\theta}}{r}, \\ (\boldsymbol{\nabla} \cdot \boldsymbol{\tau})_\theta &= \frac{\partial \tau_{\theta r}}{\partial r} + \frac{1}{r} \frac{\partial \tau_{\theta\theta}}{\partial \theta} + \frac{\partial \tau_{\theta z}}{\partial z} + \frac{2\tau_{r\theta}}{r}, \\ (\boldsymbol{\nabla} \cdot \boldsymbol{\tau})_z &= \frac{\partial \tau_{zr}}{\partial r} + \frac{1}{r} \frac{\partial \tau_{z\theta}}{\partial \theta} + \frac{\partial \tau_{zz}}{\partial z} + \frac{\tau_{zr}}{r}. \end{aligned}$$

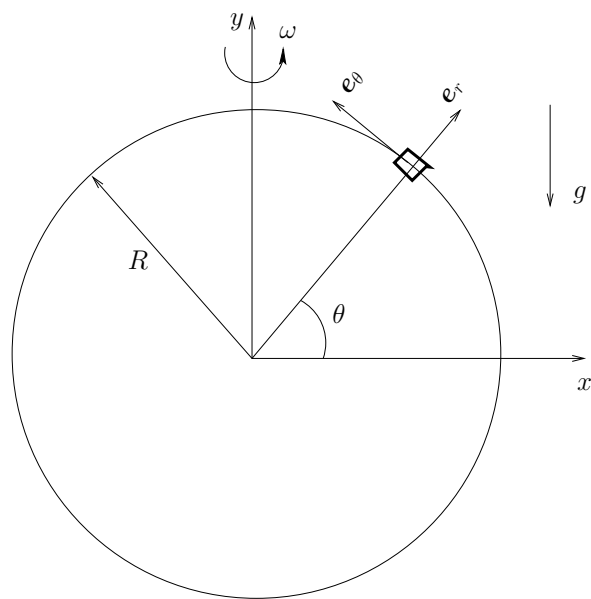


Figure 1: A small body sliding on a frictionless wire.