

Mechanics of Microsystems : Micro/nano Mechanics
(NE 211)
Course Project

Coding isothermal Reynolds equation in Matlab and comparing with analytical solution for the '0000' boundary condition

More S. K.
Cense – M.Tech

Outline

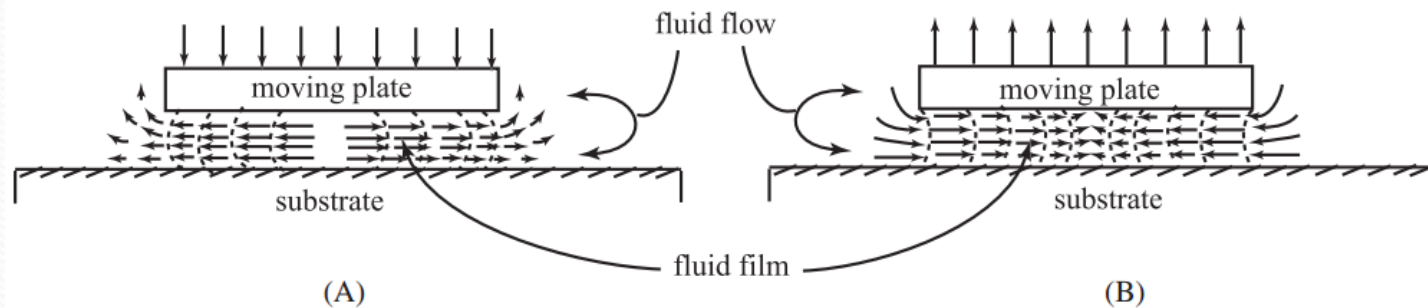
- What is Squeeze Film Damping
- What is the Governing Equation
- FE formulation
- Formulation of Matlab Code
- Results

Squeeze Film Damping

- Cavities, filled with air or some other gas, are common in MEMS.
- Squeeze film effect is natural in such devices.

Consider a air gap between movable plate and fixed underlying structure.

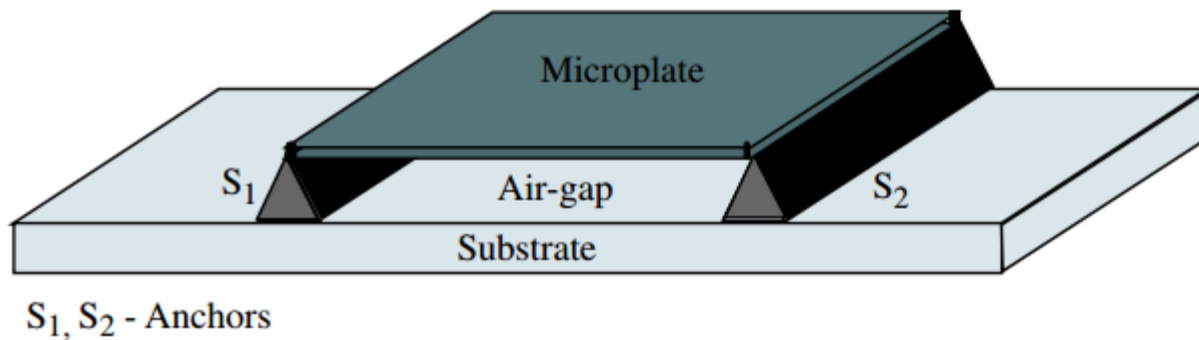
Figure 4: A schematic diagram of squeeze film flow (A) downward normal motion; (B) upward normal motion.²⁰



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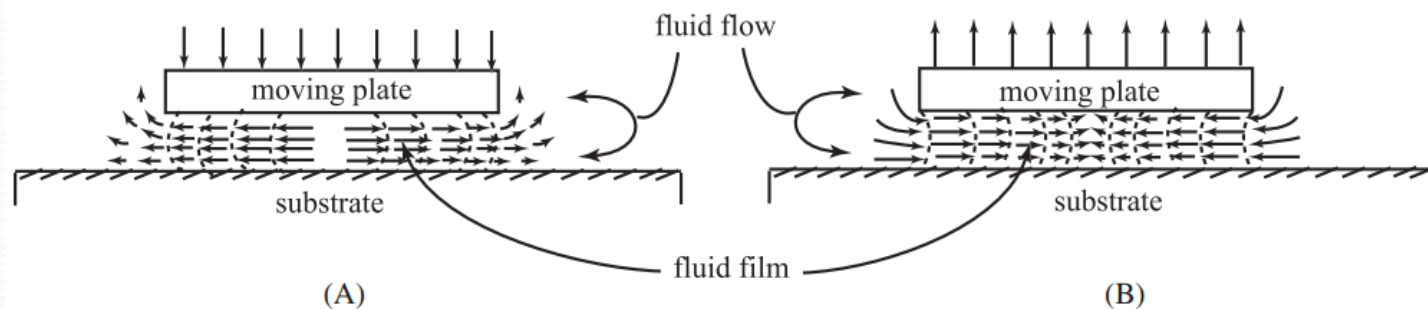
Figure 2: Schematic of a flexible structure under squeeze film damping.



Squeeze Film Damping

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Figure 4: A schematic diagram of squeeze film flow (A) downward normal motion; (B) upward normal motion.²⁰

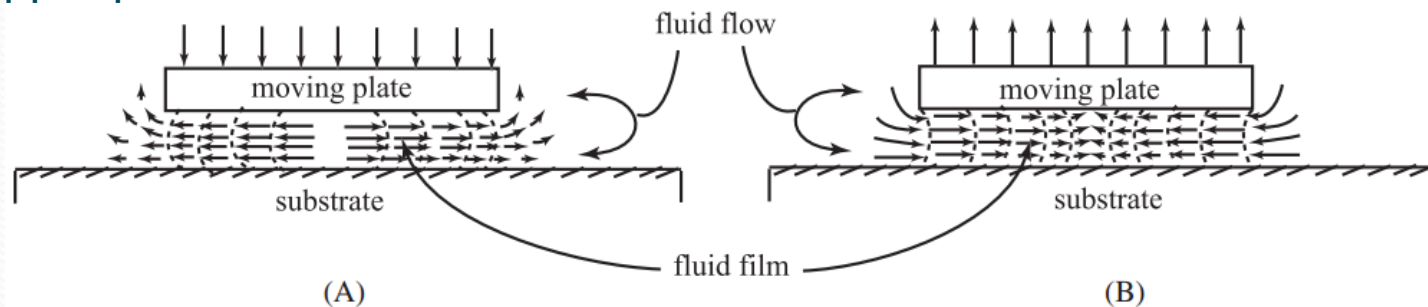


Squeeze Film Damping

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Figure 4: A schematic diagram of squeeze film flow (A) downward normal motion; (B) upward normal motion.²⁰

The upper plate moves down.

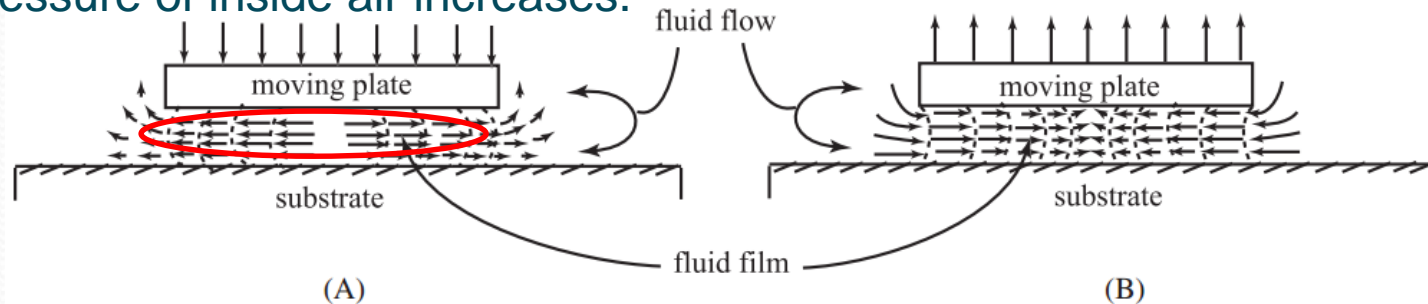


Squeeze Film Damping

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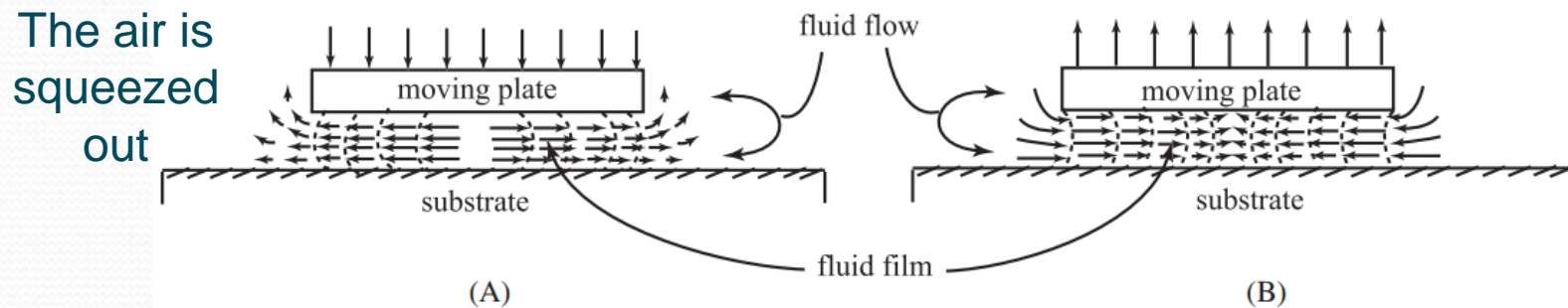
Pressure of inside air increases.



Squeeze Film Damping

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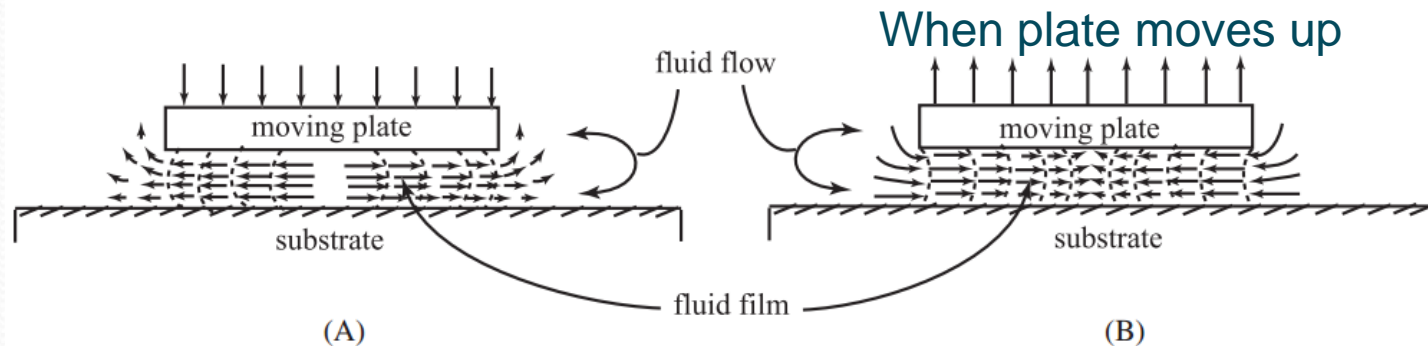
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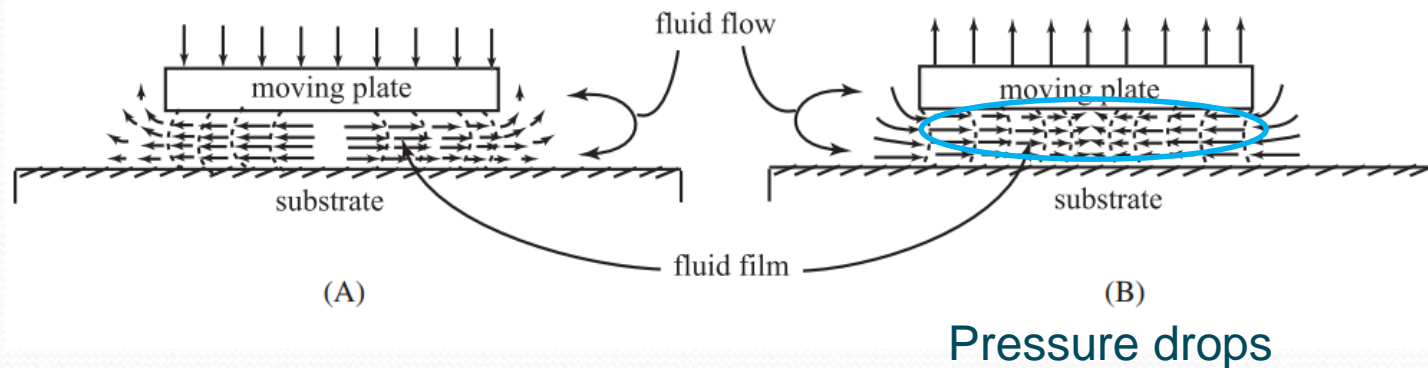
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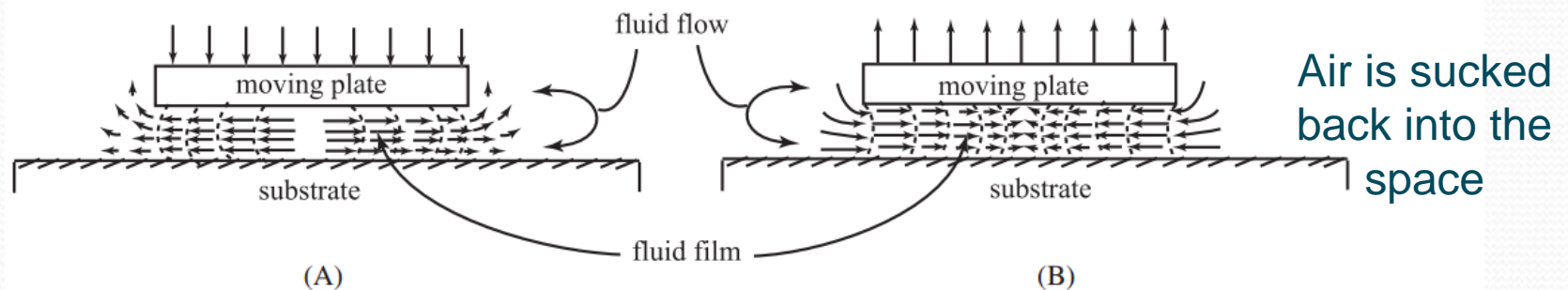
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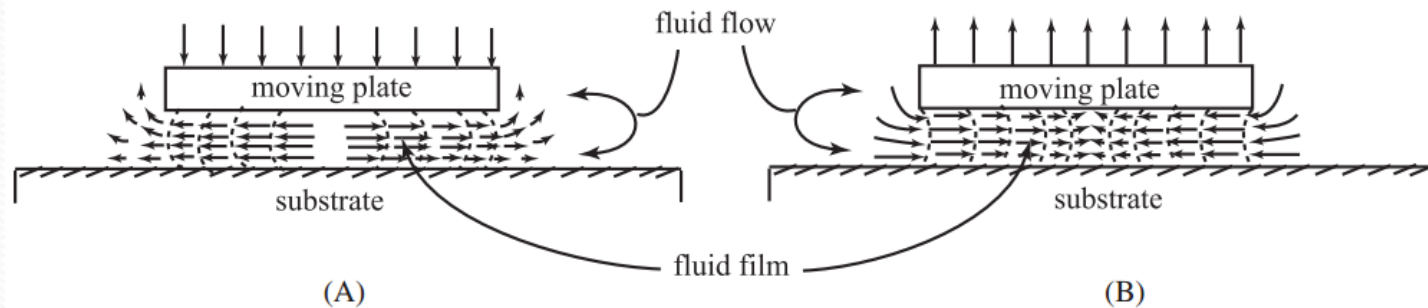


Squeeze Film Damping

The viscous drag during the flow creates a dissipative mechanical force on the plate opposing the motion.

This dissipative force is called
Squeeze Film Damping

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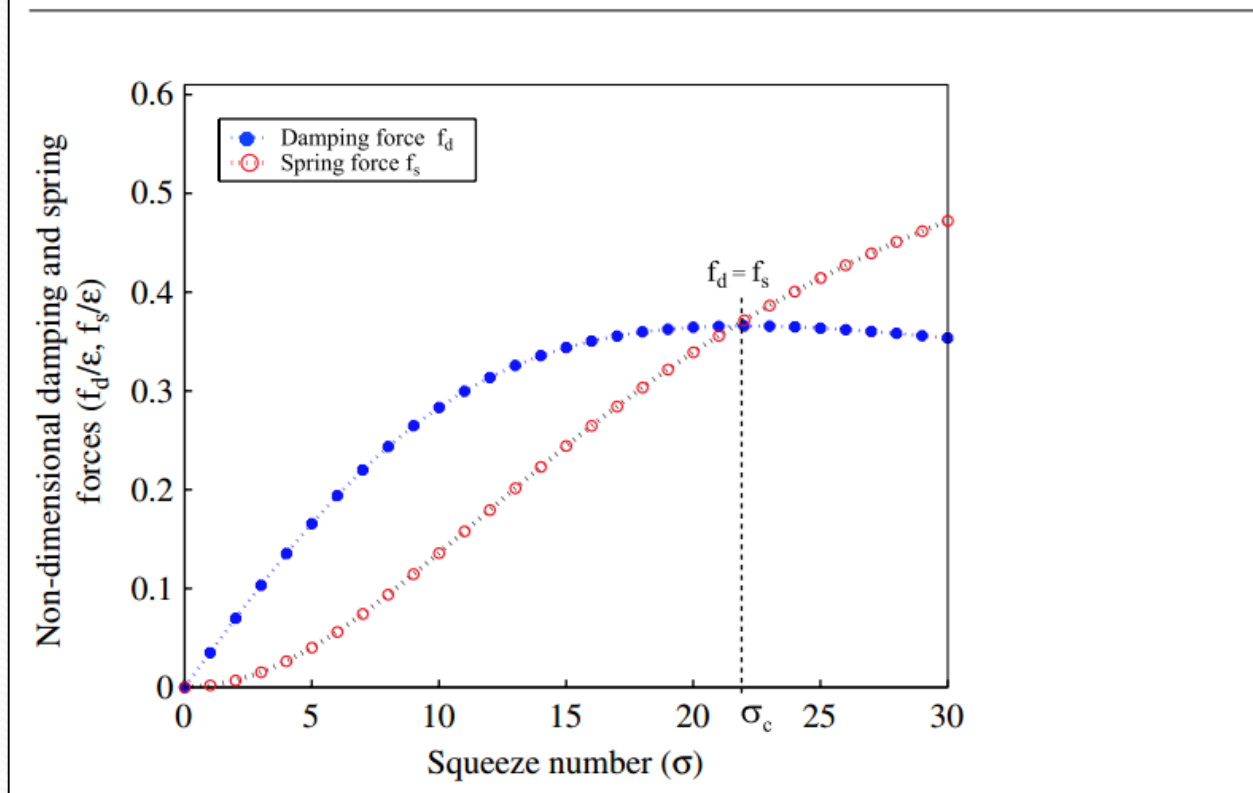


The behavior of trapped gas film at different frequencies of vibration of the plate is of particular interest

- For slow motions of moving plate the effect of the squeezed film is pure damping force, independent of pressure.
- The fluid motion is in phase with the moving plate.
- At higher frequencies of oscillations it often happens that fluid motion lags the plate motion by complete 180deg
- In such a case fluid can't escape from the cavity even if the boundary is open.
- The squeeze film behaves like a spring.

Squeeze Film Effect

Figure 6: Variation of non-dimensional damping force (f_d/ϵ) and spring force (f_s/ϵ) with squeeze number σ ; the point of intersection of the two curves (i.e., $f_d=f_s$) corresponds to the cut-off squeeze number (σ_c).



Governing Equation

Linearised Reynolds Equation

$$\frac{\partial^2 P}{\partial X^2} + \frac{\partial^2 P}{\partial Y^2} = \alpha^2 \left[\frac{\partial H}{\partial t} + \frac{\partial P}{\partial t} \right]$$

$$\alpha^2 = \frac{12 \mu}{h_0^2 \rho_a}$$

μ = effective viscosity
 ρ_a = ambient air pressure

Non Dimensionalizing by guessing solutions

$$P = \tilde{P} e^{i\omega t} \quad H = \delta \phi e^{i\omega t}$$

$$X = L x$$

$$Y = L y$$

$$\sigma = \alpha^2 L^2 \omega$$

$$\frac{\partial^2 \tilde{P}}{\partial x^2} + \frac{\partial^2 \tilde{P}}{\partial y^2} = \sigma [i\delta\phi + i\tilde{P}]$$

\tilde{P} = Pressure amplitude

ϕ = shape of plate

δ = displacement amplitude

Weak Form or Weighted Integral

$$\int \frac{\partial \tilde{p}}{\partial x_i} \frac{\partial v}{\partial x_i} d\Omega + i\delta \int (\tilde{p} + \phi\delta) v d\Omega = 0$$

v = weight function

After substituting shape functions for v and Nondimensionalized P

$$\sum_{j=1}^n \left[\int_{\Omega_e} \left\{ \frac{\partial N_i}{\partial x} \frac{\partial N_j}{\partial x} + \frac{\partial N_i}{\partial y} \frac{\partial N_j}{\partial y} + i\delta N_i N_j \right\} dx dy \right] \tilde{p}$$
$$= -i\delta \sum_{j=1}^n \left[\int_{\Omega_e} N_i N_j dx dy \right] \phi_j$$

Which can be represented in compact form as

$$[K_1 + K_2] \tilde{P} = -\delta K_2 \Phi$$

$$[K_1] = [S^{11}] + [S^{22}]$$

$$[K_2] = i \delta [S^{33}]$$

$$\begin{aligned} [S^{11}] &= \int_{\Omega_e} \frac{\partial N_i}{\partial x} \frac{\partial N_j}{\partial x} dx dy \\ &= \int_{-1}^1 \int_{-1}^1 \frac{\partial N_i}{\partial \xi} \cdot \frac{\partial N_j}{\partial \xi} d\xi d\eta \end{aligned}$$

$$\begin{aligned} [S^{33}] &= \int_{\Omega_e} N_i N_j dx dy \\ &= \int_{-1}^1 \int_{-1}^1 N_i N_j d\xi d\eta \end{aligned}$$

$$[S^{22}] = \int_{\Omega_e} \frac{\partial N_i}{\partial y} \frac{\partial N_j}{\partial y} dx dy$$

$$[S^{22}] = \int_{-1}^1 \int_{-1}^1 \frac{\partial N_i}{\partial \eta} \cdot \frac{\partial N_j}{\partial \eta} d\xi d\eta$$

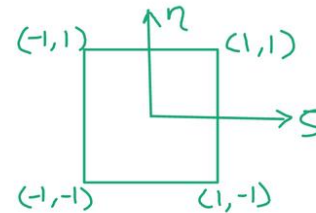
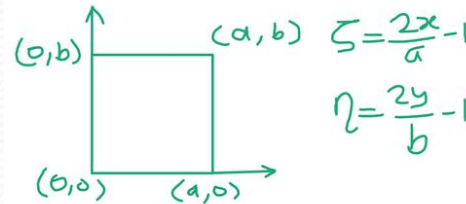
Shape Functions for Bilateral Square Element in Natural Coordinate System

$$N_1 = \frac{1}{4}(1-\xi)(1-\eta)$$

$$N_2 = \frac{1}{4}(1+\xi)(1-\eta)$$

$$N_3 = \frac{1}{4}(1+\xi)(1+\eta)$$

$$N_4 = \frac{1}{4}(1-\xi)(1+\eta)$$



And the change of Coordinates

$$\frac{\partial N}{\partial x} = \frac{\partial N}{\partial \xi} \frac{\partial \xi}{\partial x} + \frac{\partial N}{\partial \eta} \frac{\partial \eta}{\partial x}$$

$$\frac{\partial N}{\partial y} = \frac{\partial N}{\partial \xi} \frac{\partial \xi}{\partial y} + \frac{\partial N}{\partial \eta} \frac{\partial \eta}{\partial y}$$

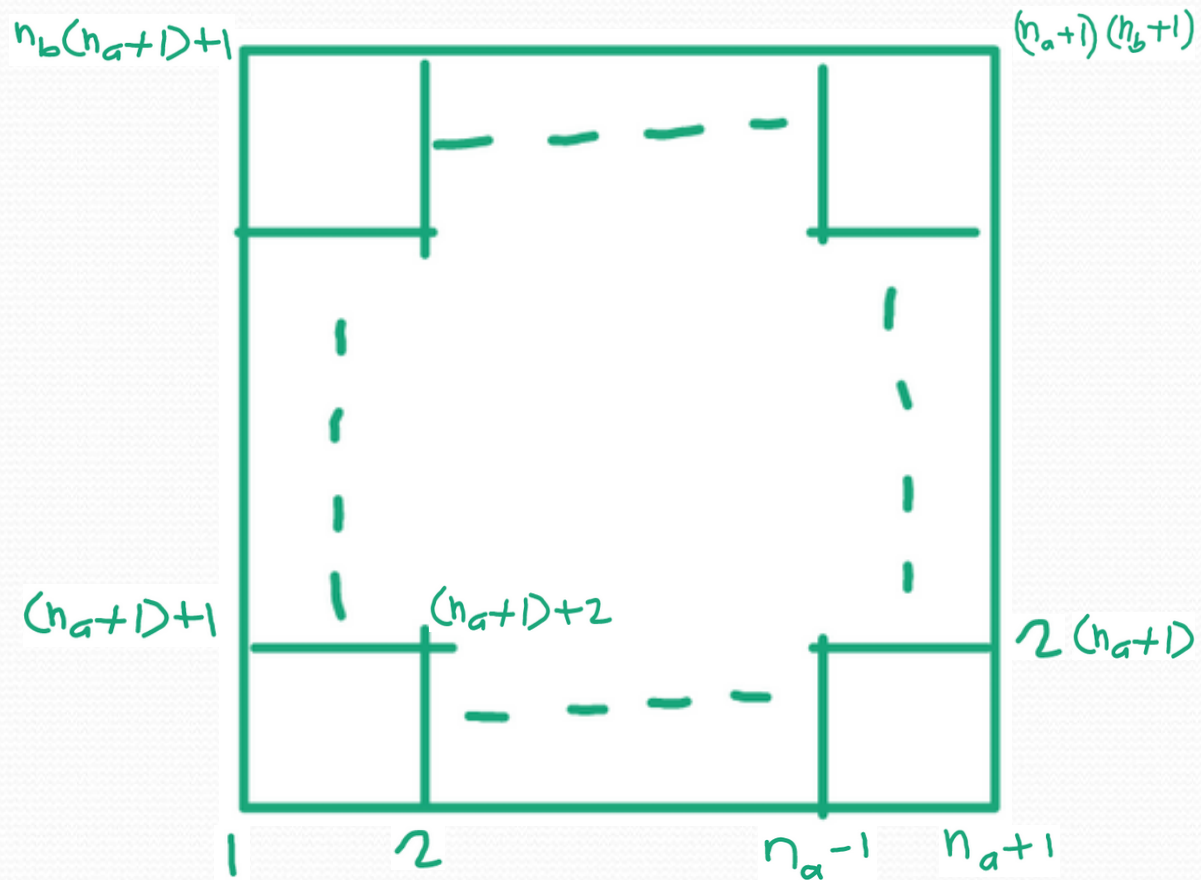
$$J = \begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{bmatrix}$$

$$dx dy = \det[J] d\xi d\eta$$

Flow Chart for FEA solution of Reynolds equation

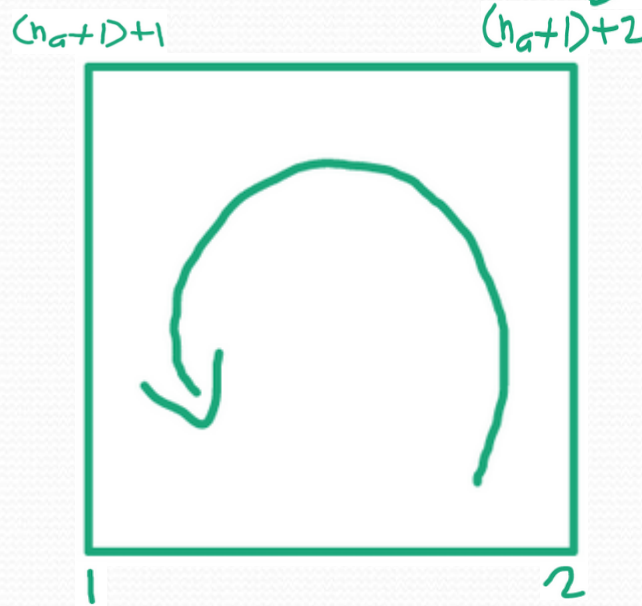
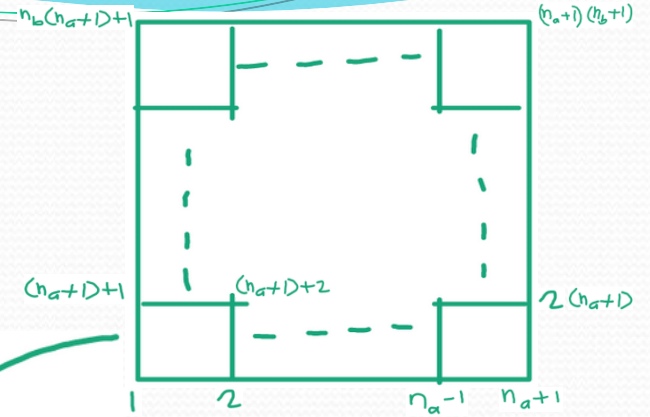
- Preprocessing
 - Node and Element Matrix
 - Contain Global and Local coordinates of nodes
 - Nodal connectivity of Elements
 - Apply Boundary Conditions
 - i.e. Save all nodes which are constrained.
 - Save all nodes other than constrained in different matrix
 - Prepare Mode Shape Matrix
 - Node Displacements according to first mode shape

- Node and Element Matrix



- Node and Element Matrix

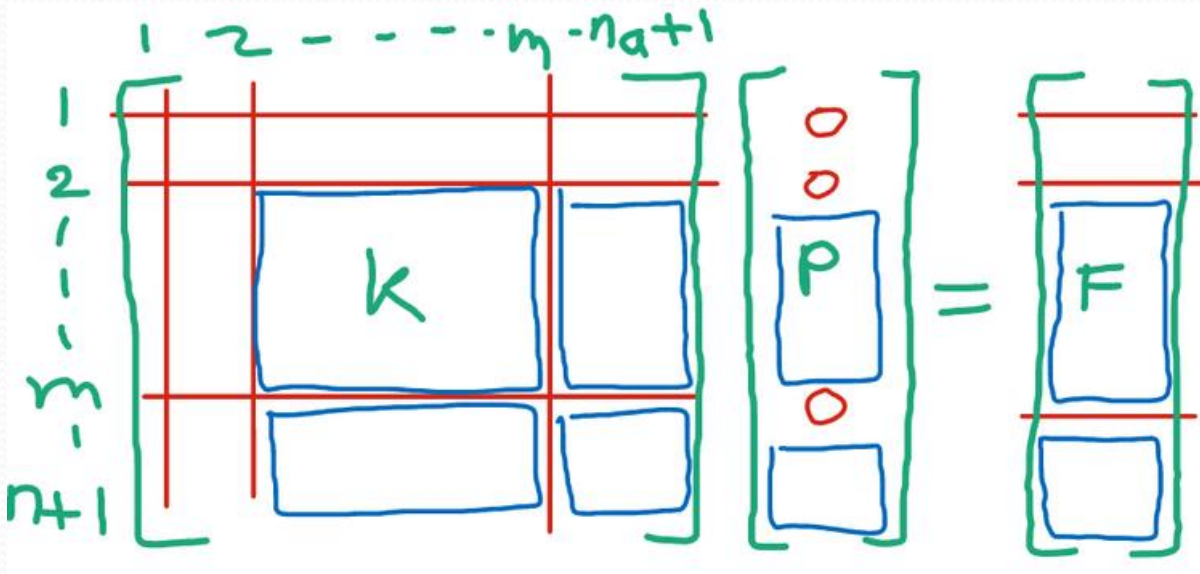
- Local Node Numbering for Elements
- Local Node Connectivity



- Building Element Matrix
 - Element Matrix for each element
 - Assembly of all element matrices in Global Matrices K_{1_g} and K_{2_g}
 - Building Global Force matrix

- Solving

- Applying Boundary Conditions.

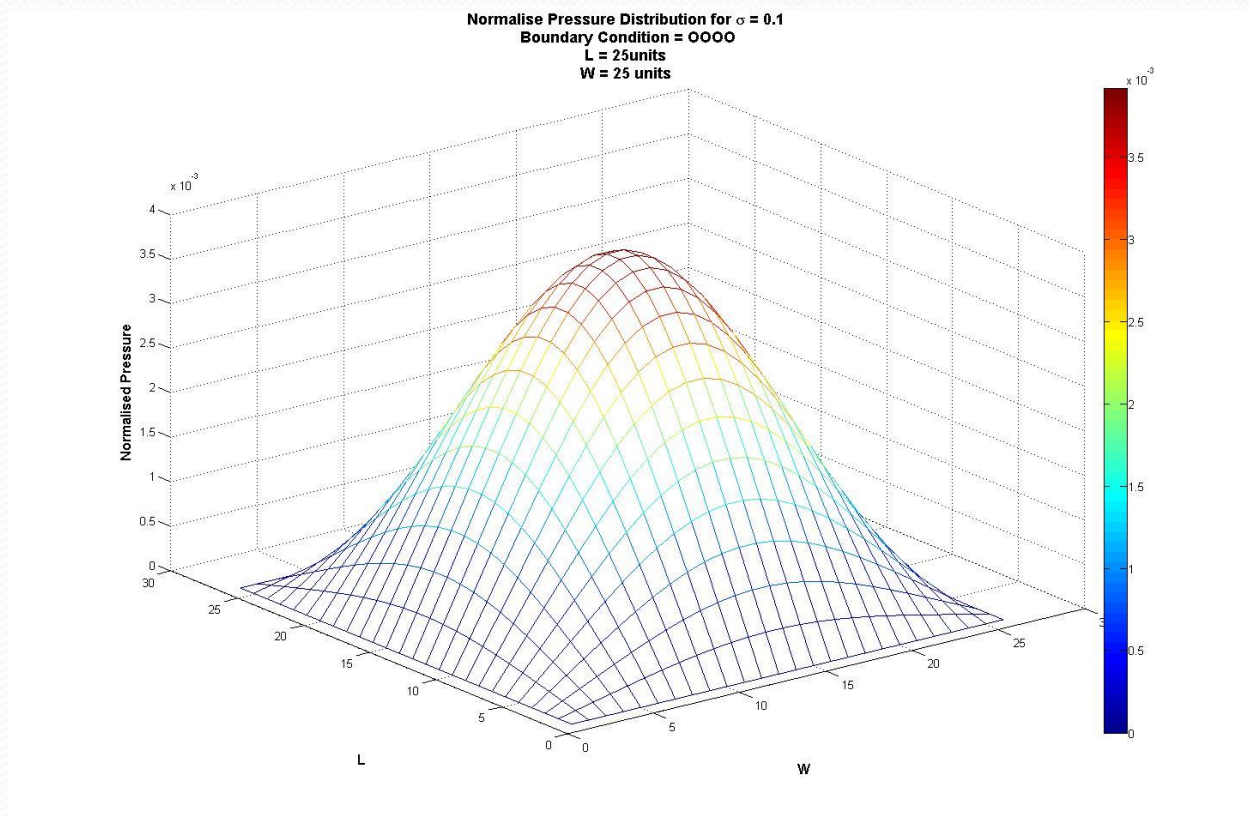


- Solving for Pressure distribution.

$$\{P\} = [K]^{-1}\{F\}$$

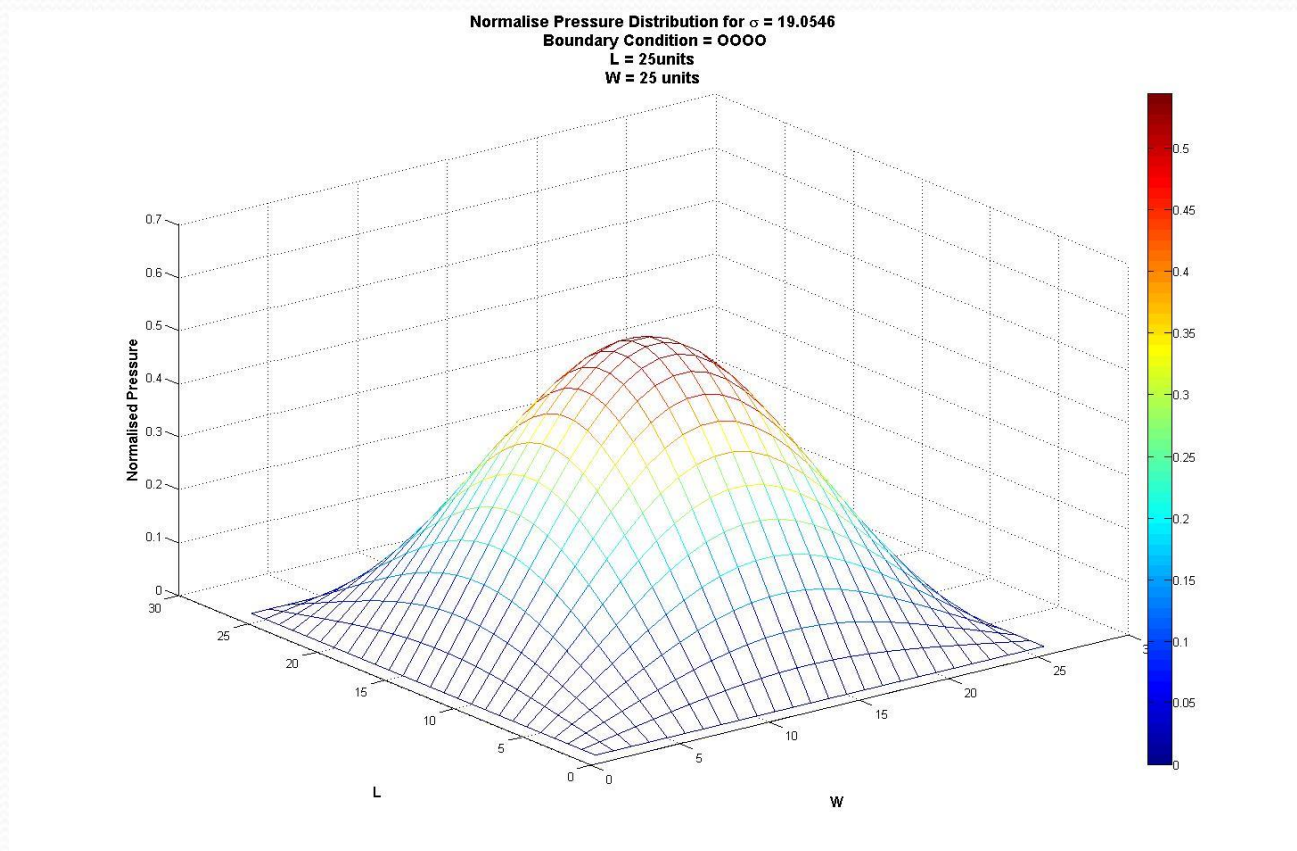
Results

- Boundary Condition = “OOOO”



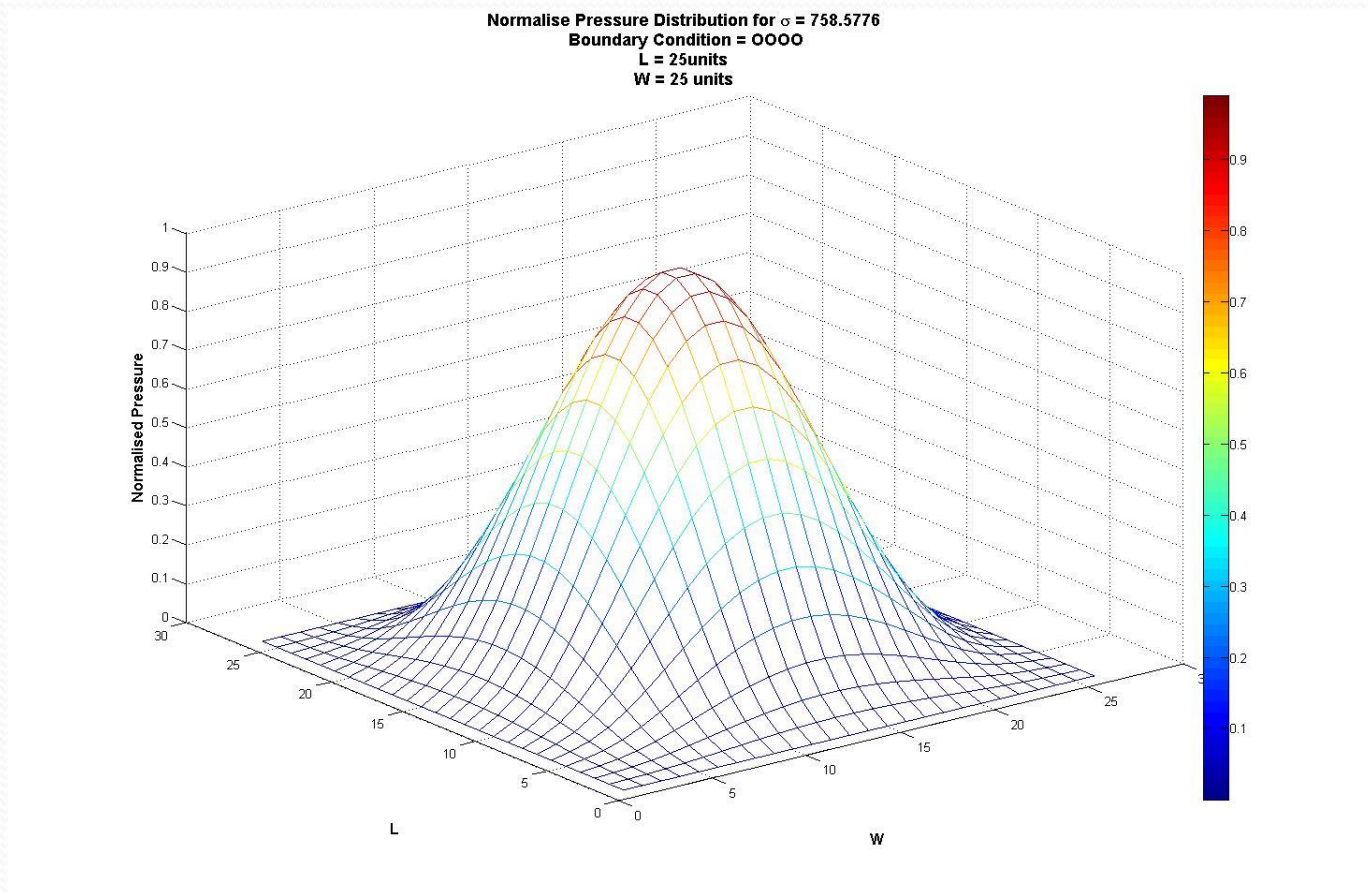
Results

- Boundary Condition = “0000”



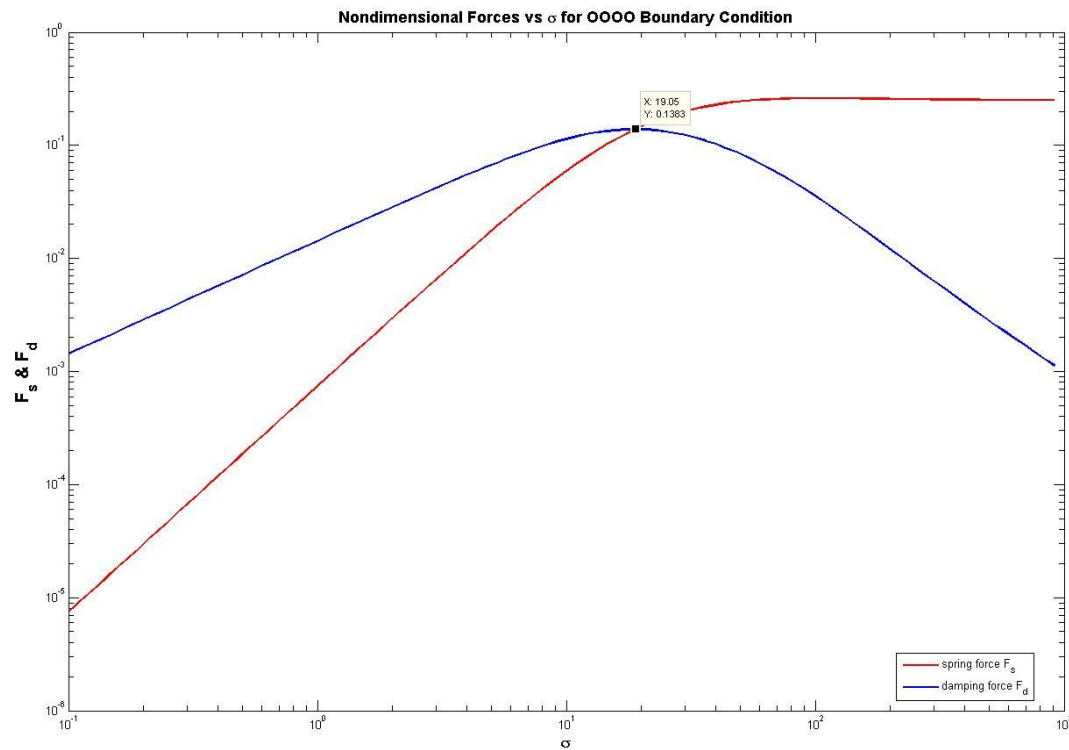
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References

- Pratap R, Mohite S, Pandey A K 2007 Squeeze Film Effects in MEMS devices *Journal of the Indian Institute of Science* VOL 87, NO 1 (2007), PP 75-94.
- A Roychowdhury, S patra Variational formulation for the Reynolds equation.
- Reddy J. N. An Introduction to Finite Element Method.
- S. D. Senturia, Micro system design

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