

**ANALYTICAL VERIFICATION
OF EQUIVALENCE OF
MAXWELL STRESS TENSOR
AND
ELECTROSTATIC SURFACE FORCE**

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OUTLINES

- Conductors and Dielectrics
- Ponderomotive force
- Equivalent Stress Tensor
- Maxwell Stress Tensor
- Striction Stress
- Traction
- Traction on Surface charge
- Traction on Surface charge of Conductor
- References



CONDUCTORS AND DIELECTRICS

- Materials can be conductors, insulators, semiconductors.

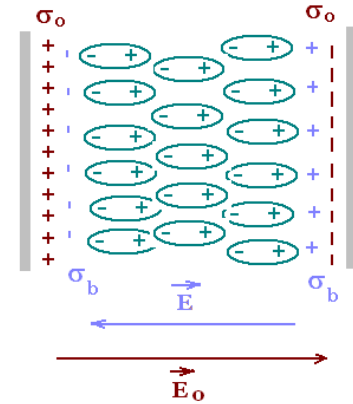


Photo: Scientific sentence

- Any charge introduced into conductor distributes itself over its surface. This displacement, though microscopic, is also found in dielectrics.
- This displacement is characterized by ‘electric displacement’ \mathbf{D} and defined as,

$$\mathbf{D} \stackrel{\text{def}}{=} \epsilon_0 \mathbf{E} + \mathbf{P} \stackrel{\text{def}}{=} \epsilon \mathbf{E}$$

\mathbf{P} is electric polarization vector, ϵ_0 is permittivity of free space, ϵ is permittivity of dielectric.



PONDEROMOTIVE FORCE

- The expression of Ponderomotive body force of an electric field is expressed as

$$\mathbf{f} = \Psi_v \mathbf{E} - \frac{1}{2} \mathbf{E} \cdot \mathbf{E} \nabla \varepsilon + \frac{1}{2} \nabla (\mathbf{E} \cdot \mathbf{E} \frac{\partial \varepsilon}{\partial \rho_m} \rho_m)$$

ρ_m is the mass density of dielectric.

- Total force applied on the body

$$\mathbf{F} = \int_V \mathbf{f} dV$$

Assumptions :

1. Value of ε changes smoothly in the interfaces of different media.
2. Surface free charge is absent.
3. V is total electric field.



EQUIVALENT STRESS TENSOR

- Let $\boldsymbol{\tau}_e$ denote stress tensor equivalent to body force. So,

$$\mathbf{F} = \int_V \mathbf{f} dV = \oint_S \boldsymbol{\tau}_e \mathbf{n} dS$$

$$\mathbf{N} = \int_V \mathbf{R} \times \mathbf{f} dV = \oint_S \mathbf{R} \times (\boldsymbol{\tau}_e \mathbf{n}) dS$$

where \mathbf{F} and \mathbf{N} denotes total force and total moment.

- Total moment equality makes $\boldsymbol{\tau}_e$ to be symmetric.
- \mathbf{f} is decomposed into two components

$$\mathbf{f} = \mathbf{f}_1 + \mathbf{f}_2, \text{ where } \mathbf{f}_1 = \Psi_v \mathbf{E} - \frac{1}{2} \mathbf{E} \cdot \mathbf{E} \boldsymbol{\nabla} \varepsilon$$
$$\text{and } \mathbf{f}_2 = \frac{1}{2} \boldsymbol{\nabla} (\mathbf{E} \cdot \mathbf{E} \frac{\partial \varepsilon}{\partial \rho_m} \rho_m)$$



MAXWELL STRESS TENSOR

○ Now, $f_{1x} = (\nabla \cdot \mathbf{D})E_x - \frac{1}{2} \mathbf{E} \cdot \mathbf{E} \frac{\partial \varepsilon}{\partial x}$

$$(\nabla \cdot \mathbf{D})E_x = \nabla \cdot (E_x \mathbf{D}) - \mathbf{D} \nabla \cdot E_x$$

$$\text{and } \mathbf{D} \nabla \cdot E_x = \varepsilon \mathbf{E} \nabla \cdot E_x = \frac{\varepsilon}{2} \frac{\partial \mathbf{E} \cdot \mathbf{E}}{\partial x}$$

○ Hence, $f_{1x} = \frac{\partial (E_x D_x - \frac{\varepsilon}{2} \mathbf{E} \cdot \mathbf{E})}{\partial x} + \frac{\partial E_x D_y}{\partial y} + \frac{\partial E_x D_z}{\partial z}$

○ Similarly, $f_{1y} = \frac{\partial E_y D_x}{\partial x} + \frac{\partial (E_y D_y - \frac{\varepsilon}{2} \mathbf{E} \cdot \mathbf{E})}{\partial y} + \frac{\partial E_y D_z}{\partial z}$

$$f_{1z} = \frac{\partial E_z D_x}{\partial x} + \frac{\partial E_z D_y}{\partial y} + \frac{\partial (E_z D_z - \frac{\varepsilon}{2} \mathbf{E} \cdot \mathbf{E})}{\partial z}$$

○ Tensor $\boldsymbol{\tau}_{em}$ corresponding to \mathbf{f}_1 is termed as Maxwell stress tensor.

$$\boldsymbol{\tau}_{em} = \varepsilon (\mathbf{E} \otimes \mathbf{E} - \frac{1}{2} (\mathbf{E} \cdot \mathbf{E}) \mathbf{I})$$



STRICTION STRESS

- Tensor $\boldsymbol{\tau}_{es}$ corresponding to \boldsymbol{f}_2 is striction tensor

$$\boldsymbol{\tau}_{es} = \frac{1}{2} (\boldsymbol{E} \cdot \boldsymbol{E} \frac{\partial \varepsilon}{\partial \rho_m} \rho_m) \boldsymbol{I}$$

- Equivalent stress tensor, $\boldsymbol{\tau}_e = \boldsymbol{\tau}_{es} + \boldsymbol{\tau}_{em}$
- If we are not interested in the distribution of Ponderomotive forces over the volume of an arbitrary body, but only their resultant, it is sufficient to consider only Maxwell's force and stress.
 - Condition: The body is surrounded by a liquid dielectric in mechanical equilibrium or vacuum.



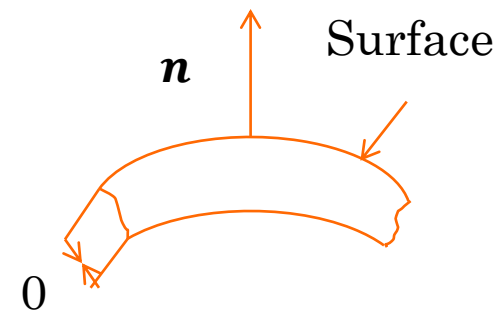
TRACTION

- The traction on a surface element with unit normal \mathbf{n} is

$$\mathbf{t} = \boldsymbol{\tau}_e \mathbf{n} = \varepsilon E_n \mathbf{E} - \frac{1}{2} \mathbf{E} \cdot \mathbf{E} \left(\varepsilon - \frac{\partial \varepsilon}{\partial \rho_m} \rho_m \right) \mathbf{n}$$

$$\mathbf{t}_m = \boldsymbol{\tau}_{em} \mathbf{n} = \varepsilon E_n \mathbf{E} - \frac{\varepsilon}{2} \mathbf{E} \cdot \mathbf{E} \mathbf{n}$$

- Surface charge is a discontinuity.
- The traction on this discontinuity can be derived from above traction by considering charged layer of finite thickness, then passing over in limit to an infinitely thin layer.

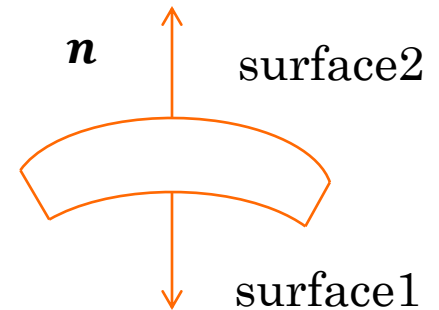


TRACTION ON SURFACE CHARGE

- $t_{1n}dS = -\varepsilon_1(E_{1n}\mathbf{E}_1 - \frac{1}{2}\mathbf{E}_1 \cdot \mathbf{E}_1 \mathbf{n})dS$
- $t_{2n}dS = \varepsilon_2(E_{2n}\mathbf{E}_2 - \frac{1}{2}\mathbf{E}_2 \cdot \mathbf{E}_2 \mathbf{n})dS$
- Net traction on this thick layer,

$$\begin{aligned}\mathbf{t} &= \mathbf{t}_{2n} - \mathbf{t}_{1n} \\ &= \varepsilon_2 \left(E_{2n}\mathbf{E}_2 - \frac{1}{2}\mathbf{E}_2 \cdot \mathbf{E}_2 \mathbf{n} \right) \\ &\quad + \varepsilon_1 \left(E_{1n}\mathbf{E}_1 - \frac{1}{2}\mathbf{E}_1 \cdot \mathbf{E}_1 \mathbf{n} \right)\end{aligned}$$

- This relation also holds in the limit.



TRACTION ON SURFACE CHARGE OF CONDUCTOR

- For Metal $\mathbf{E}_1 = \mathbf{0}$, $\mathbf{E}_2 = E_2 \mathbf{n}$

$$\mathbf{t} = \epsilon_2 \left(\frac{1}{2} E_2 E_2 \right) \mathbf{n}$$

- Taking a gaussian surface on the surface of conductor,

$$\epsilon_2 E_2 = \Psi_s$$

$$\mathbf{t} = \epsilon_2 \left(\frac{1}{2} E_2 E_2 \right) \mathbf{n} = \frac{1}{2} \frac{\Psi_s^2}{\epsilon_2} \mathbf{n}$$

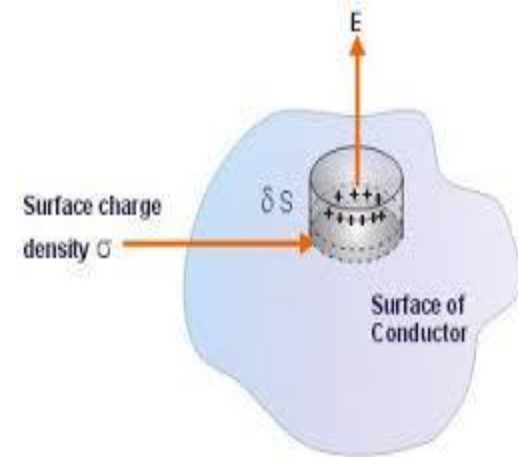


Photo: <http://onlinephys.com/>

