

ME 254

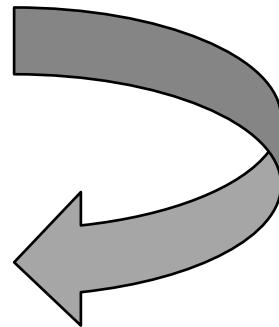
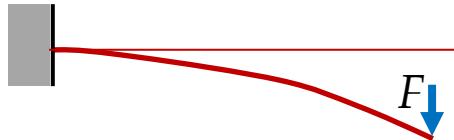
*Elastic similarity* calculations  
using elliptic integrals in Matlab

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# Important equations

$$\int_0^{\theta_L} \frac{d\theta}{\sqrt{2 \frac{F}{EI} (\sin \theta_L - \sin \theta)}} = \int_0^L ds = L$$



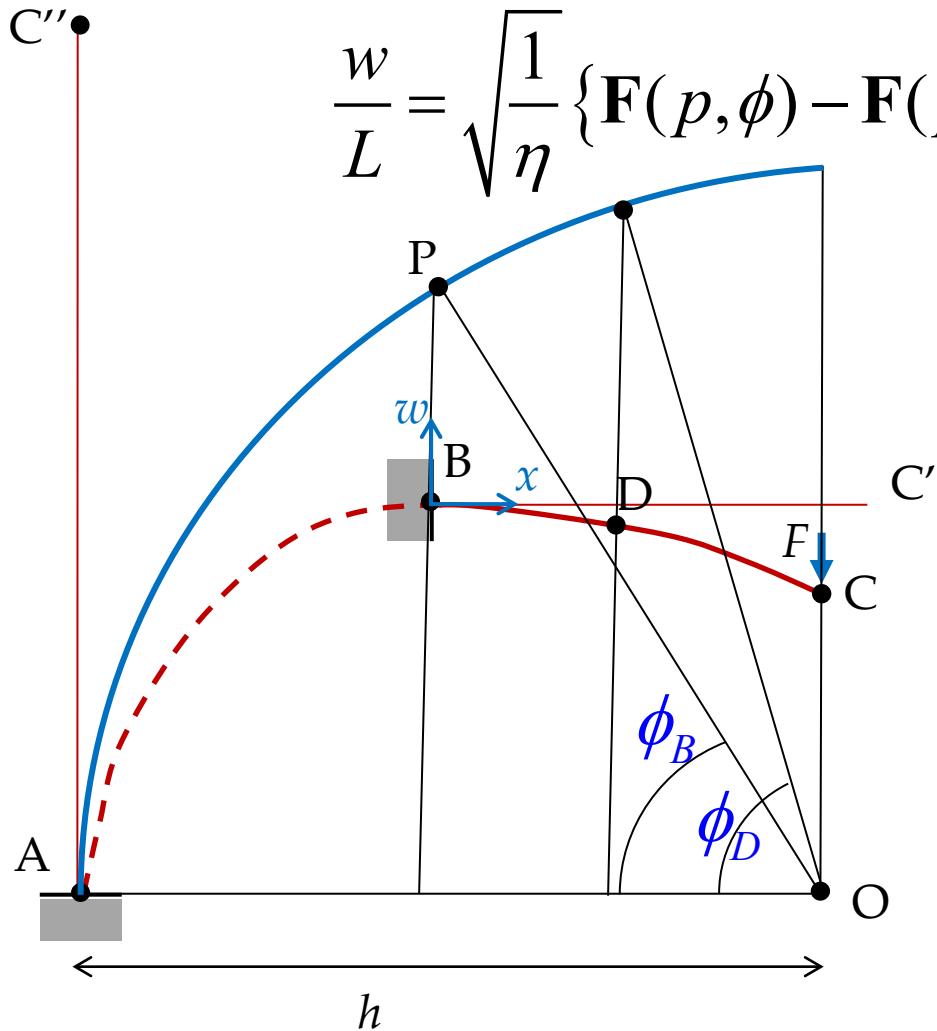
$$\theta \rightarrow \phi$$

$$\sin \theta = 2 p^2 \sin^2 \phi - 1$$

$$p^2 = \frac{1 + \sin \theta_L}{2}$$

$$\int_{\sin^{-1}\left(\frac{1}{p\sqrt{2}}\right)}^{\pi/2} \frac{d\phi}{\sqrt{\frac{F}{EI} \sqrt{1 - p^2 \sin^2 \phi}}} = L$$

# Coordinates of the deflected profile at any point beyond B



$$\frac{w}{L} = \sqrt{\frac{1}{\eta}} \left\{ \mathbf{F}(p, \phi) - \mathbf{F}(p, \phi_B) - 2\mathbf{E}(p, \phi) + 2\mathbf{E}(p, \phi_B) \right\}$$

$$\frac{x}{L} = \frac{2p}{\sqrt{\eta}} (\cos \phi_B - \cos \phi)$$

$$h = \frac{2pL}{\sqrt{\eta}} = \frac{2p}{\sqrt{F/EI}}$$

# Non-dimensional portrayal

$$\int_{\phi_1}^{\phi_2} \frac{d\phi}{\sqrt{\frac{F}{EI}} \sqrt{1 - p^2 \sin^2 \phi}} = \int_{s_1}^{s_2} ds = s_2 - s_1$$

$$\frac{w_2 - w_1}{L} = \sqrt{\frac{1}{\eta}} \left\{ \mathbf{F}(p, \phi_2) - \mathbf{F}(p, \phi_1) - 2\mathbf{E}(p, \phi_2) + 2\mathbf{E}(p, \phi_1) \right\}$$

$$\frac{x_2 - x_1}{L} = \frac{2p}{\sqrt{\frac{F}{EI}}} (\cos \phi_2 - \cos \phi_1)$$

# A numerical example



$$L = 1 \text{ m}$$

$$E = 210E9 \text{ Pa}$$

$$I = \frac{bd^3}{12}$$

$$b = 5 \times 10^{-2} \text{ m}$$

$$d = 1 \times 10^{-3} \text{ m}$$

The force varies from 0 to 12 N.

**What we use:**

Our codes:

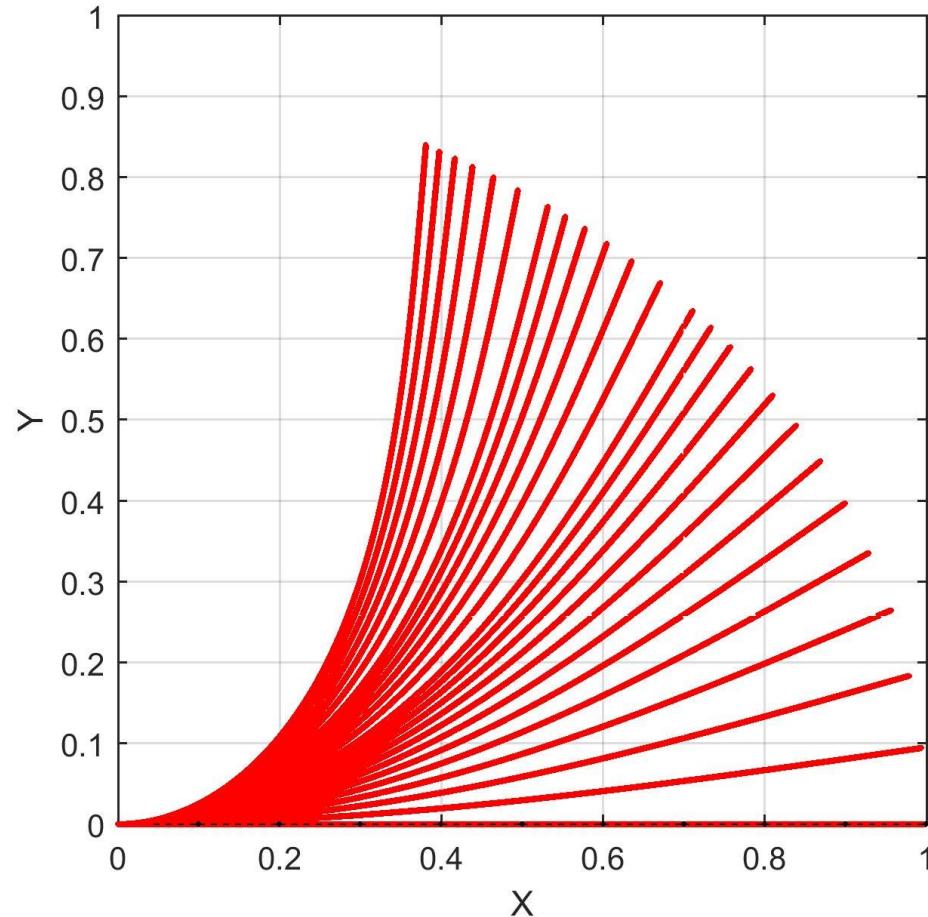
`nlbeam.m` and other files  
its data files

Matlab functions

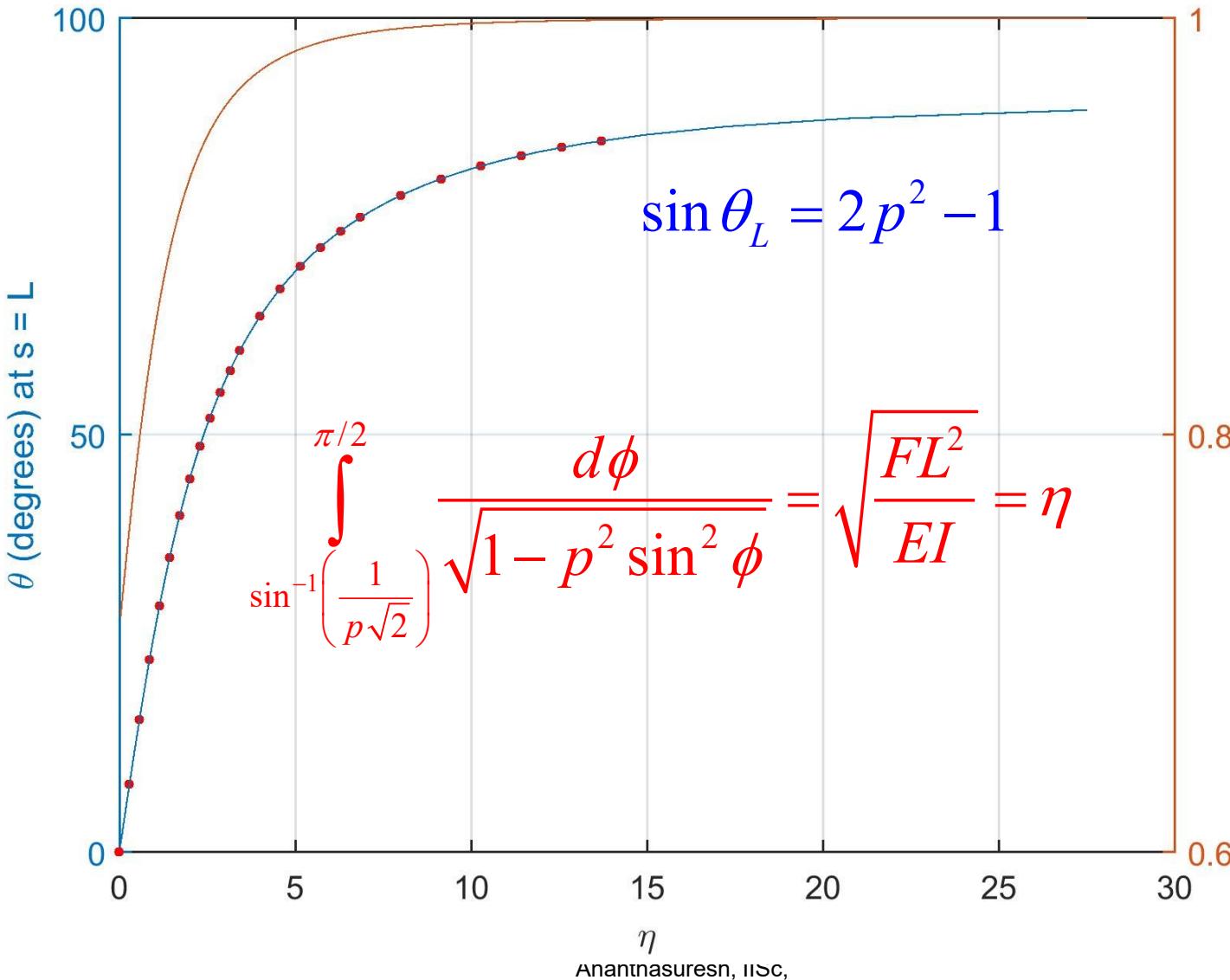
`ellipticF`  
`ellipticE`

# nlfeambeam.m code

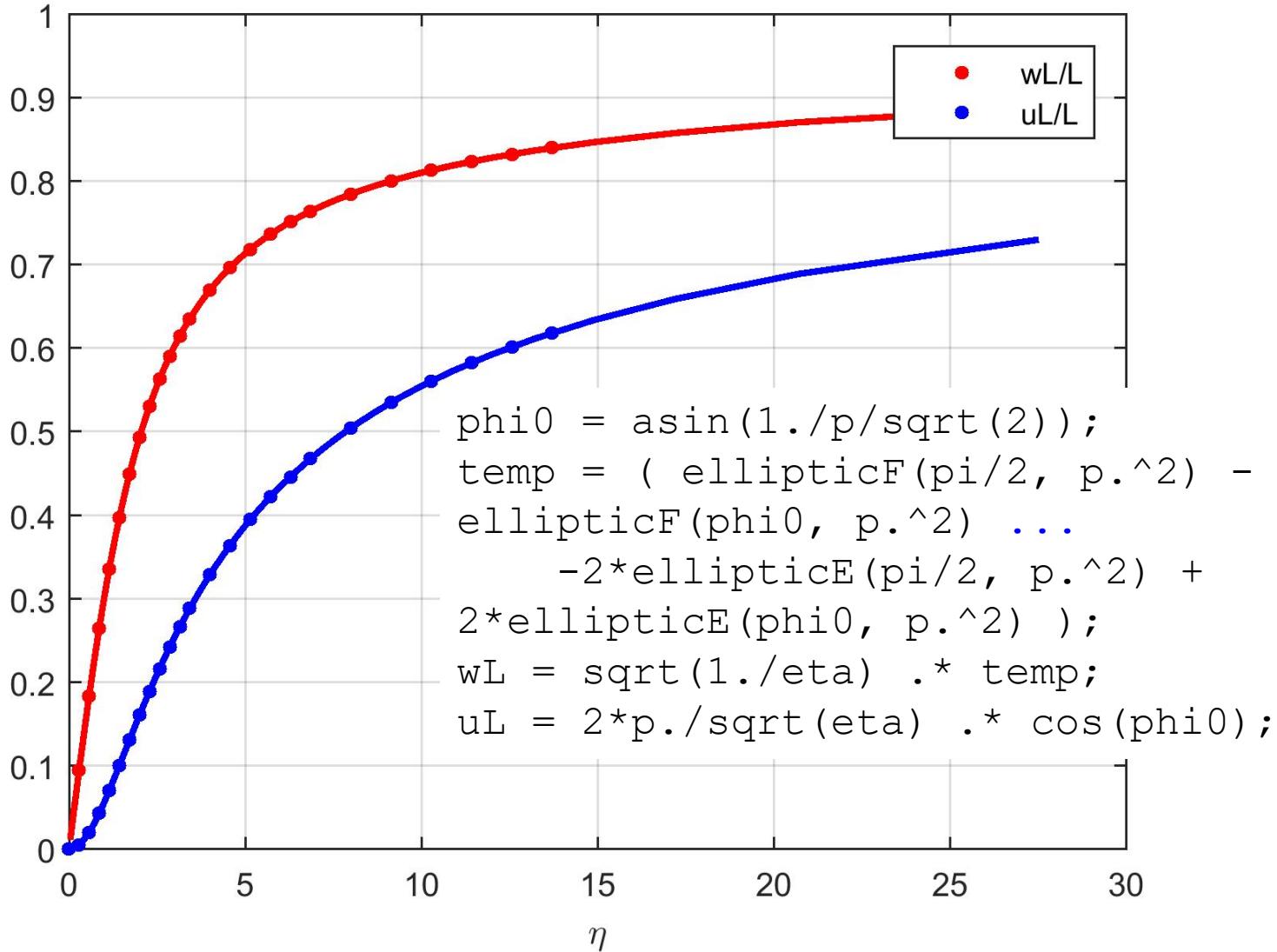
```
f = [0:0.25:3 3.5:0.5:6 7:1:12];
```



# FEA and Elliptic integral solutions



# Locus of the loaded tip

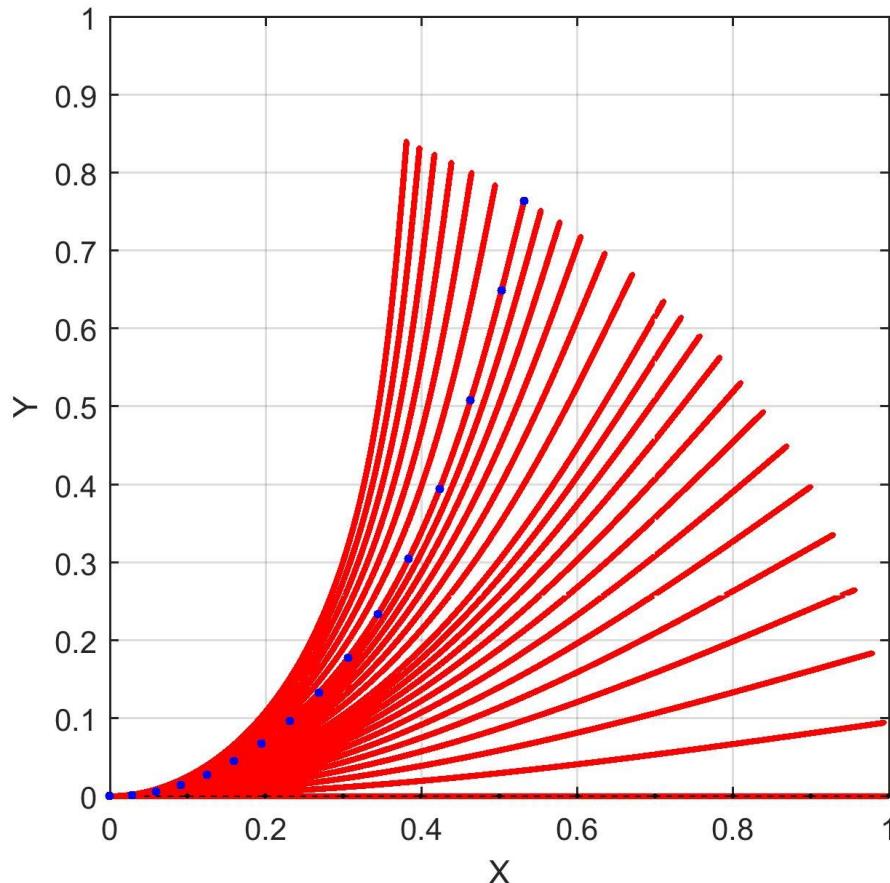


# Matlab code using elliptic integrals

```
for thetaL = pi/180:pi/180:89*pi/180,  
    i = i + 1;  
    p(i) = sqrt((1+sin(thetaL))/2);  
    phi0 = asin(1/p(i)/sqrt(2));  
    eta(i) = ( ellipticF(pi/2,p(i)^2)  
- ellipticF(phi0, p(i)^2) )^2;  
    thetaLdeg(i) = thetaL*180/pi;  
end
```

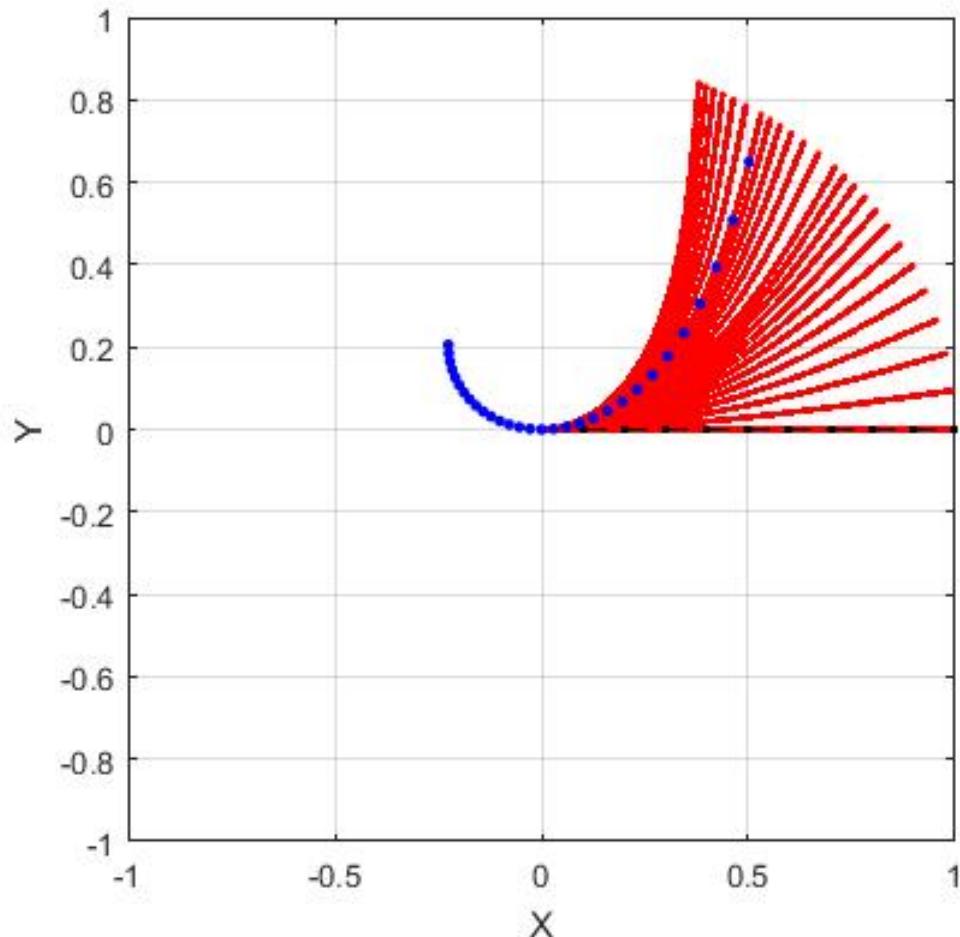
# FEA and elliptic solutions

$$\frac{w}{L} = \sqrt{\frac{1}{\eta}} \{ \mathbf{F}(p, \phi) - \mathbf{F}(p, \phi_B) - 2\mathbf{E}(p, \phi) + 2\mathbf{E}(p, \phi_B) \}$$

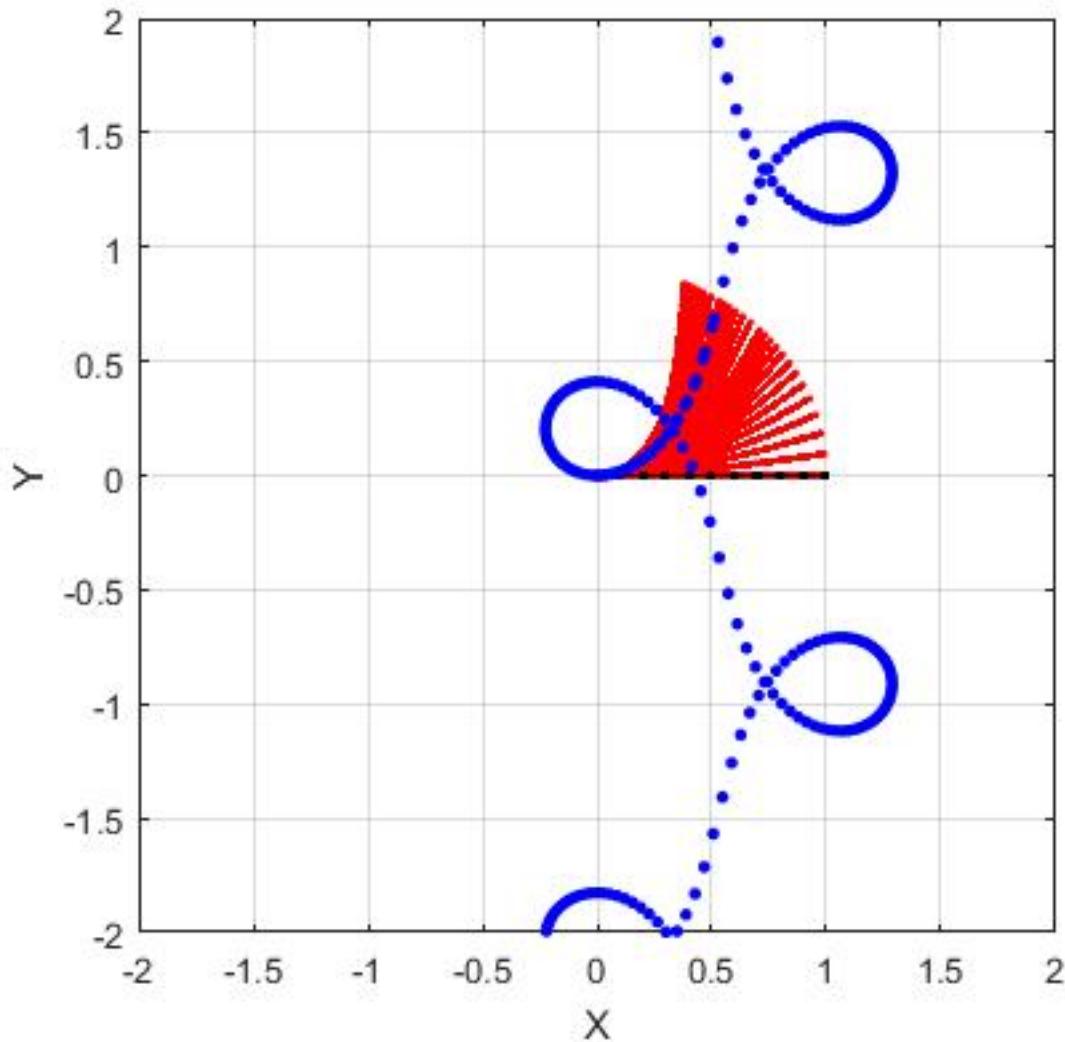


$$\frac{x}{L} = \frac{2p}{\sqrt{\eta}} (\cos \phi_B - \cos \phi)$$

# Extrapolation to a column using elastic similarity

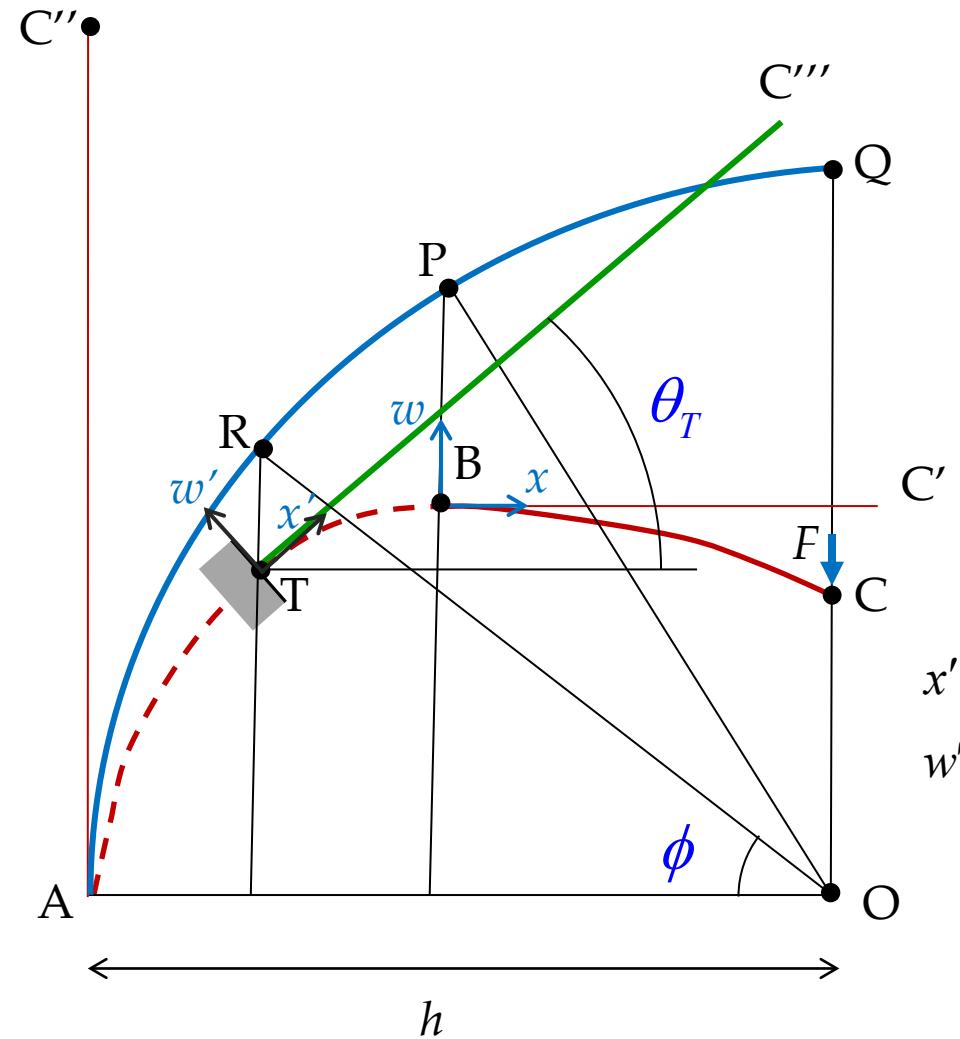
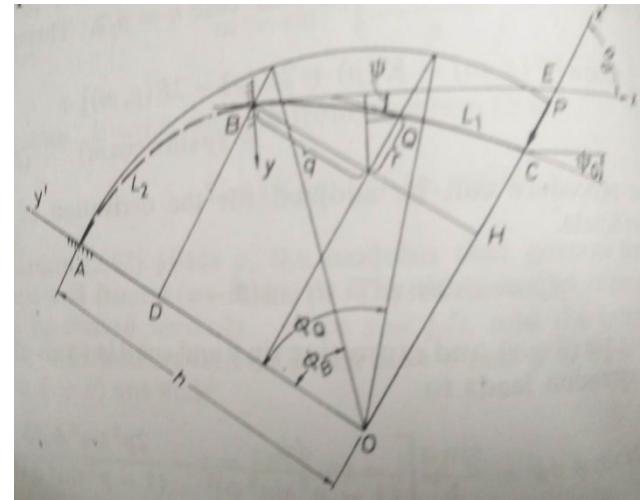


# Nodal elastica



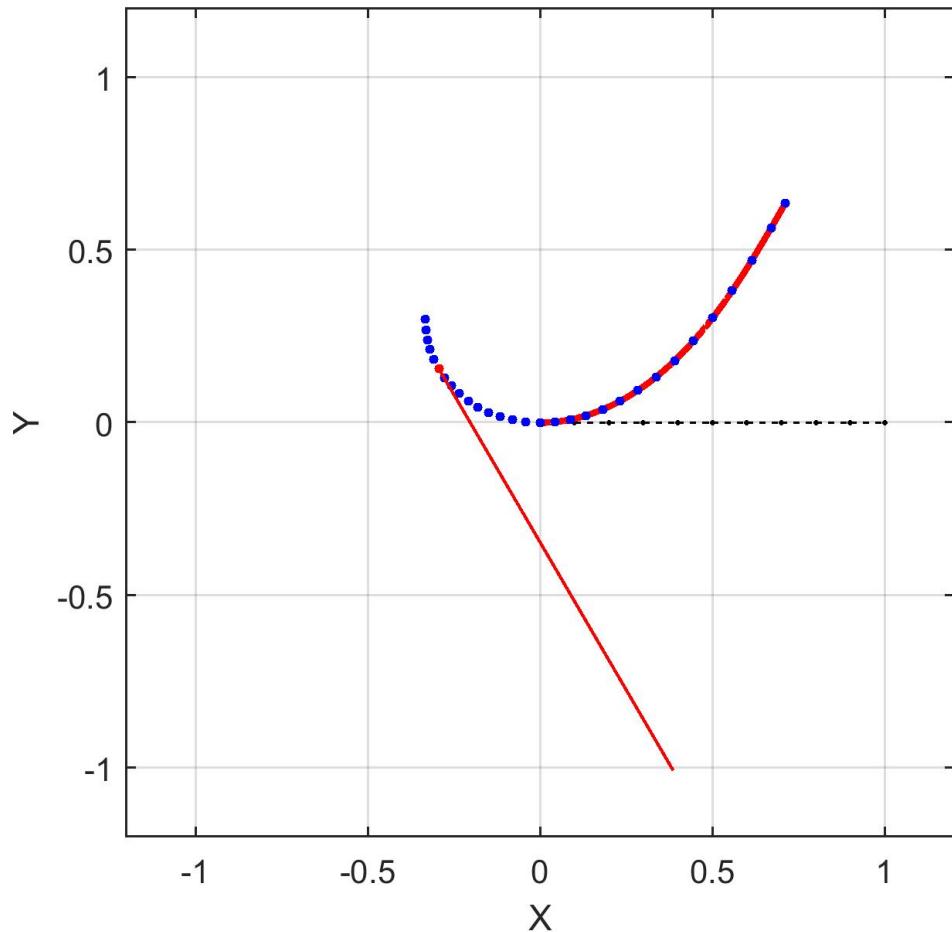
# Inclined load

Frisch-Fay, R., *Flexible Bars*, 1962.



$$\begin{aligned}x' &= x \cos \theta_T + w \sin \theta_T - (x_T \cos \theta_T + w_T \sin \theta_T) \\w' &= -x \sin \theta_T + w \cos \theta_T - (-x_T \sin \theta_T + w_T \cos \theta_T)\end{aligned}$$

# Solution for the inclined load



```
>> theta*180/pi
```

ans =

-59.7263

```
>> Lphi
```

Lphi =

1.3485

```
>> f*cos(theta)
```

ans =

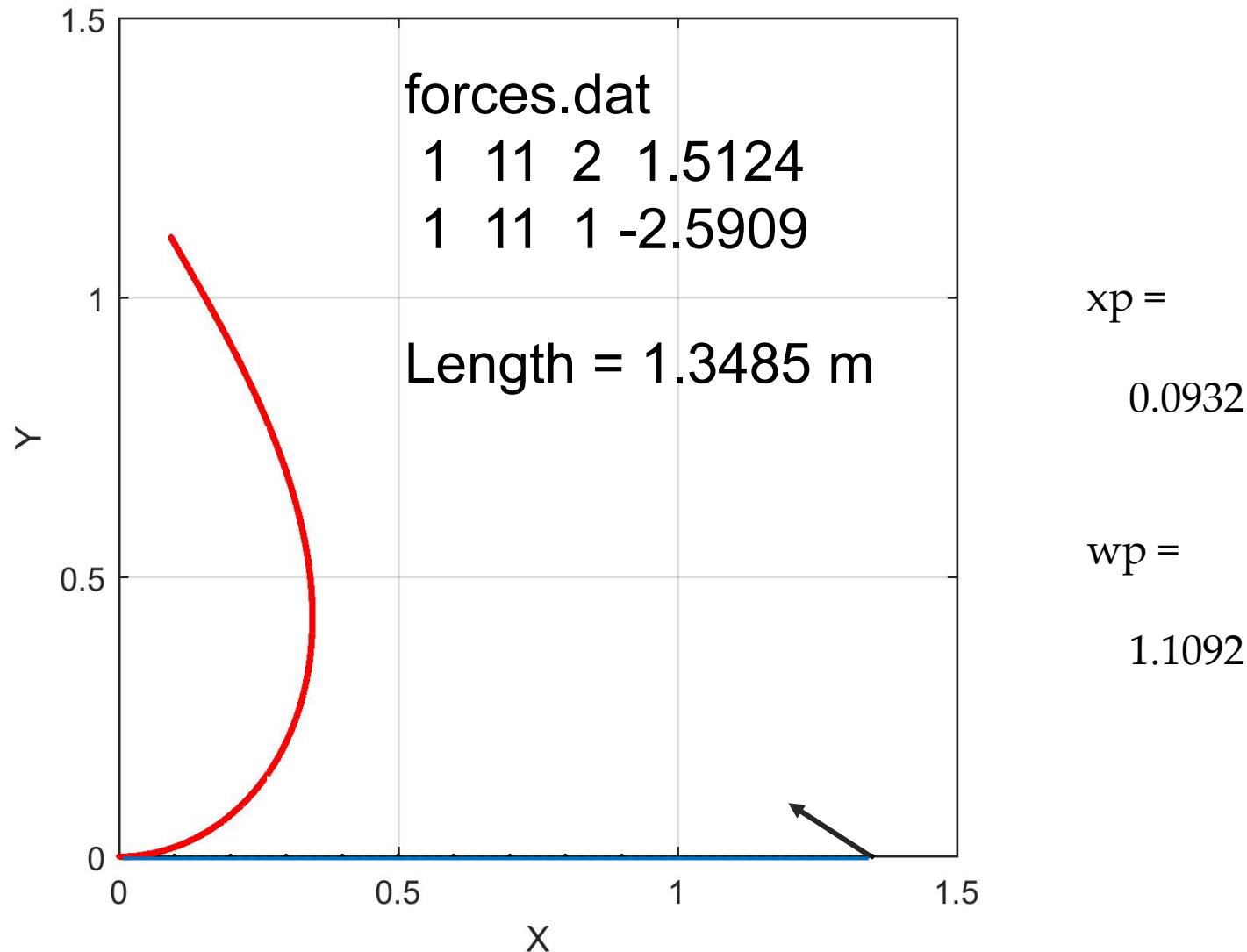
1.5124

```
>> f*sin(theta)
```

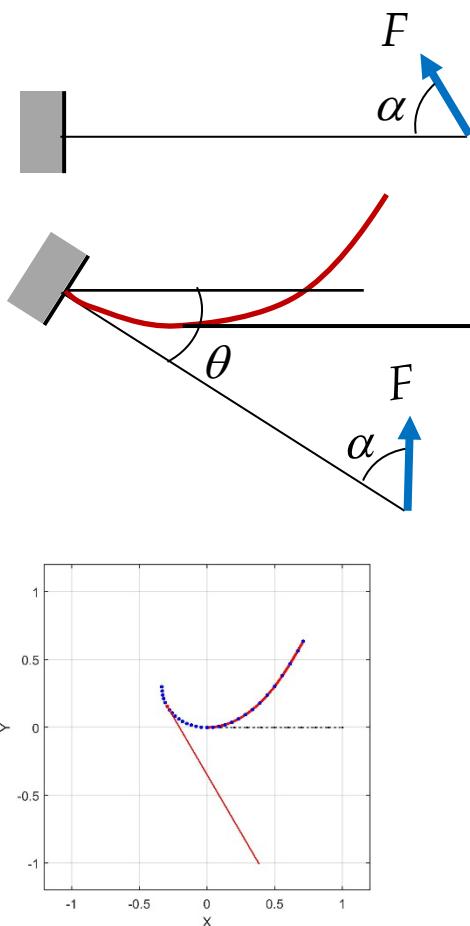
ans =

-2.5909

# FEA with the inclined load



# How do we proceed with an inclined load for a beam of length $L'$ ?



$$\theta = \frac{\pi}{2} - \alpha$$

$$\phi = \sin^{-1} \left( \sqrt{\frac{1 + \sin \theta}{2 p^2}} \right)$$

Find  $p$  such that

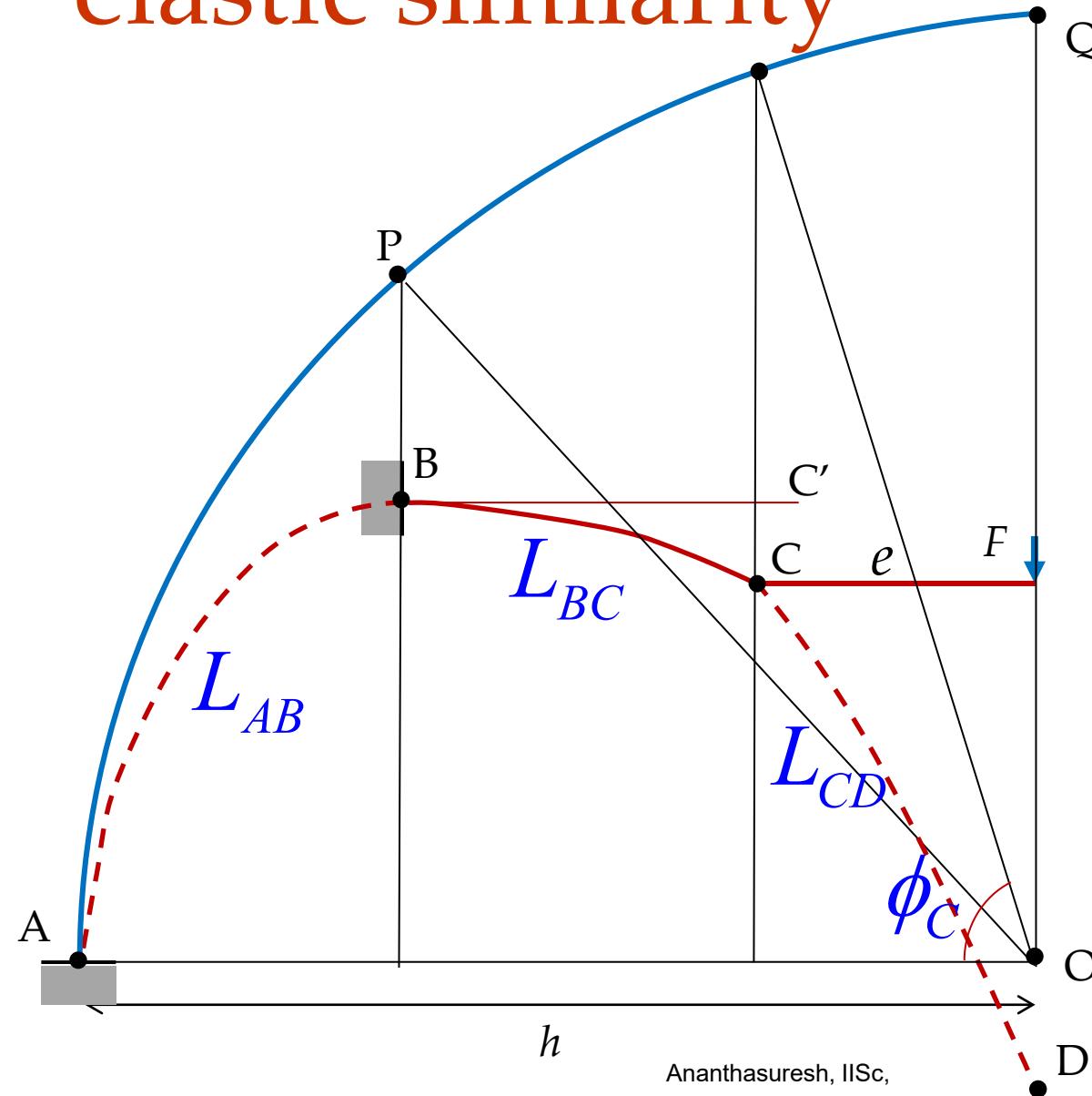
$$\int_{\phi}^{\pi/2} \frac{d\phi}{\sqrt{\frac{F}{EI} \sqrt{1 - p^2 \sin^2 \phi}}} = L'$$

Then,

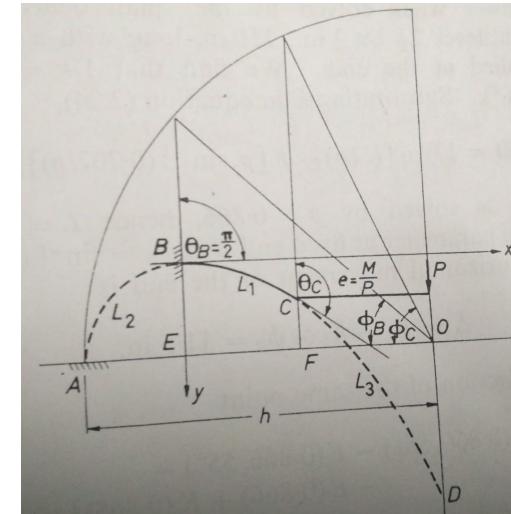
$$L = \int_{\sin^{-1} \left( \frac{1}{p\sqrt{2}} \right)}^{\pi/2} \frac{d\phi}{\sqrt{\frac{F}{EI} \sqrt{1 - p^2 \sin^2 \phi}}}$$

Let us consider a moment load now.

# Moment load added using elastic similarity



Frisch-Fay, R., *Flexible Bars*, 1962.



$$e = \frac{M}{F}$$

$$\frac{e}{h} = \cos \phi_C = \frac{e}{2p} \sqrt{\frac{F}{EI}}$$

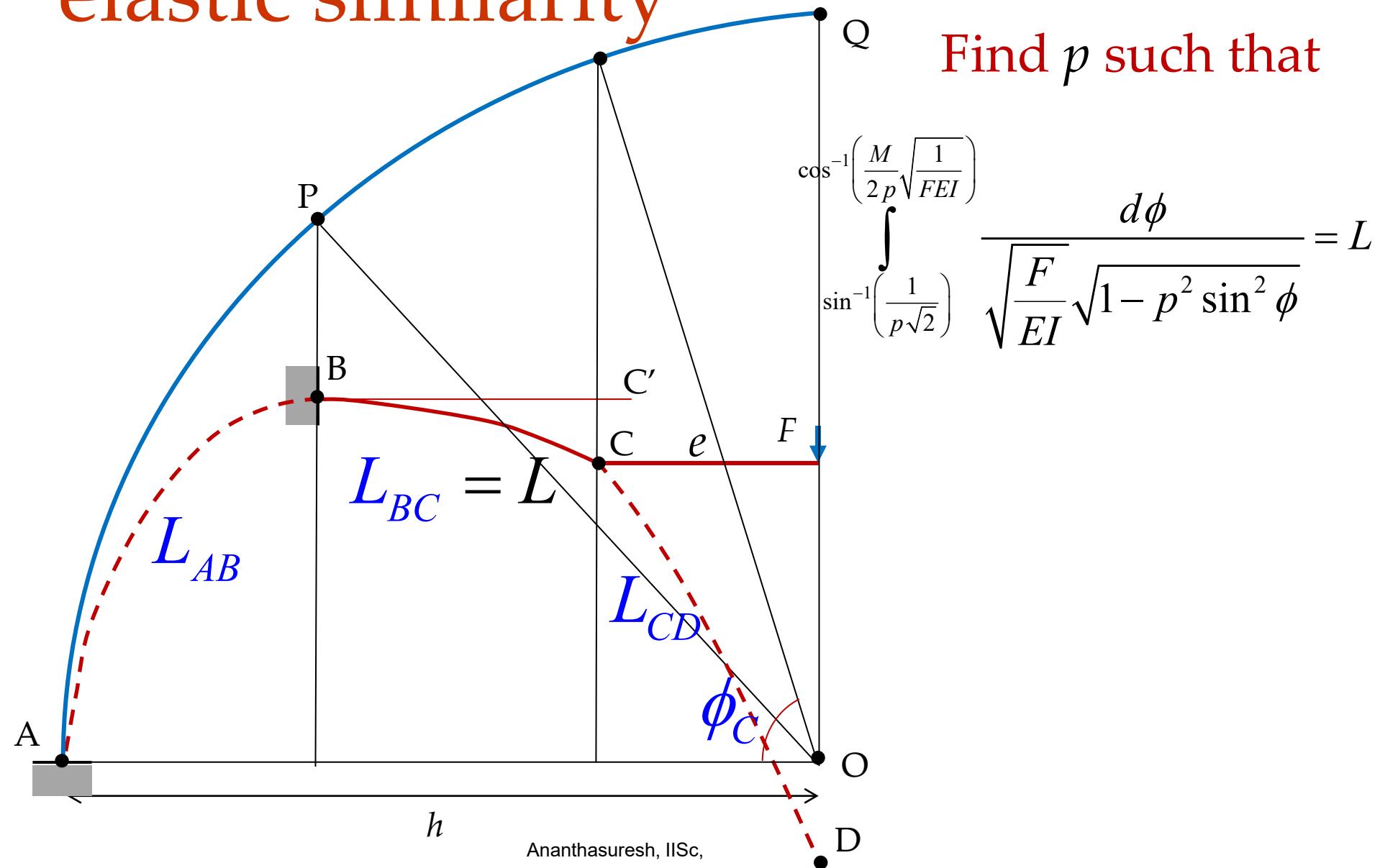
$$\phi_C = \cos^{-1} \left( \frac{M}{2p} \sqrt{\frac{1}{FEI}} \right)$$

# Moment load added using elastic similarity

Find  $p$  such that

$$\cos^{-1}\left(\frac{M}{2p}\sqrt{\frac{1}{FEI}}\right)$$

$$\sin^{-1}\left(\frac{1}{p\sqrt{2}}\right) \frac{d\phi}{\sqrt{\frac{F}{EI}}\sqrt{1-p^2\sin^2\phi}} = L$$



# An example with transverse and moment loads

forces.dat

1	11	2	3
1	11	3	0.4

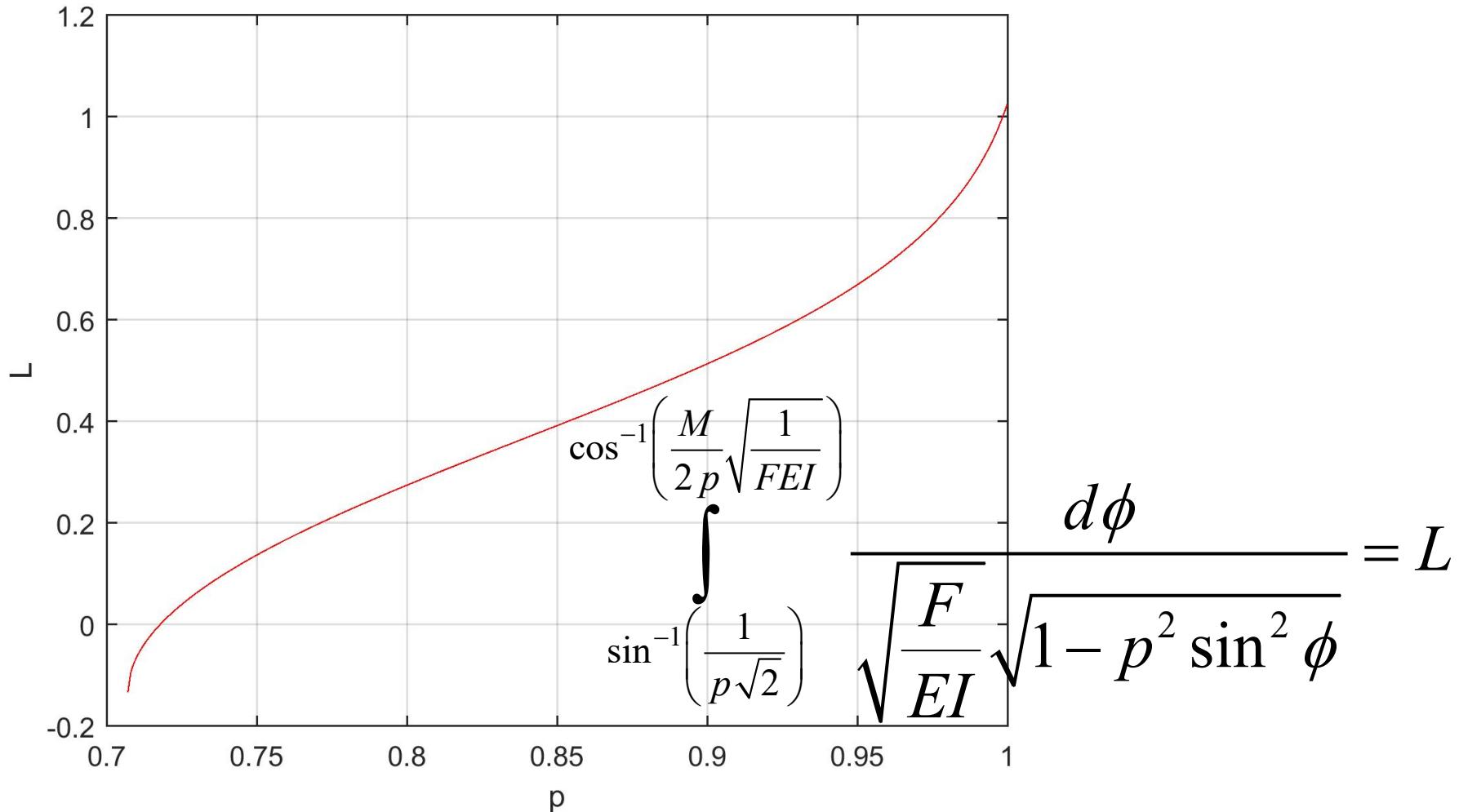
L = 1 m

E = 210 GPa

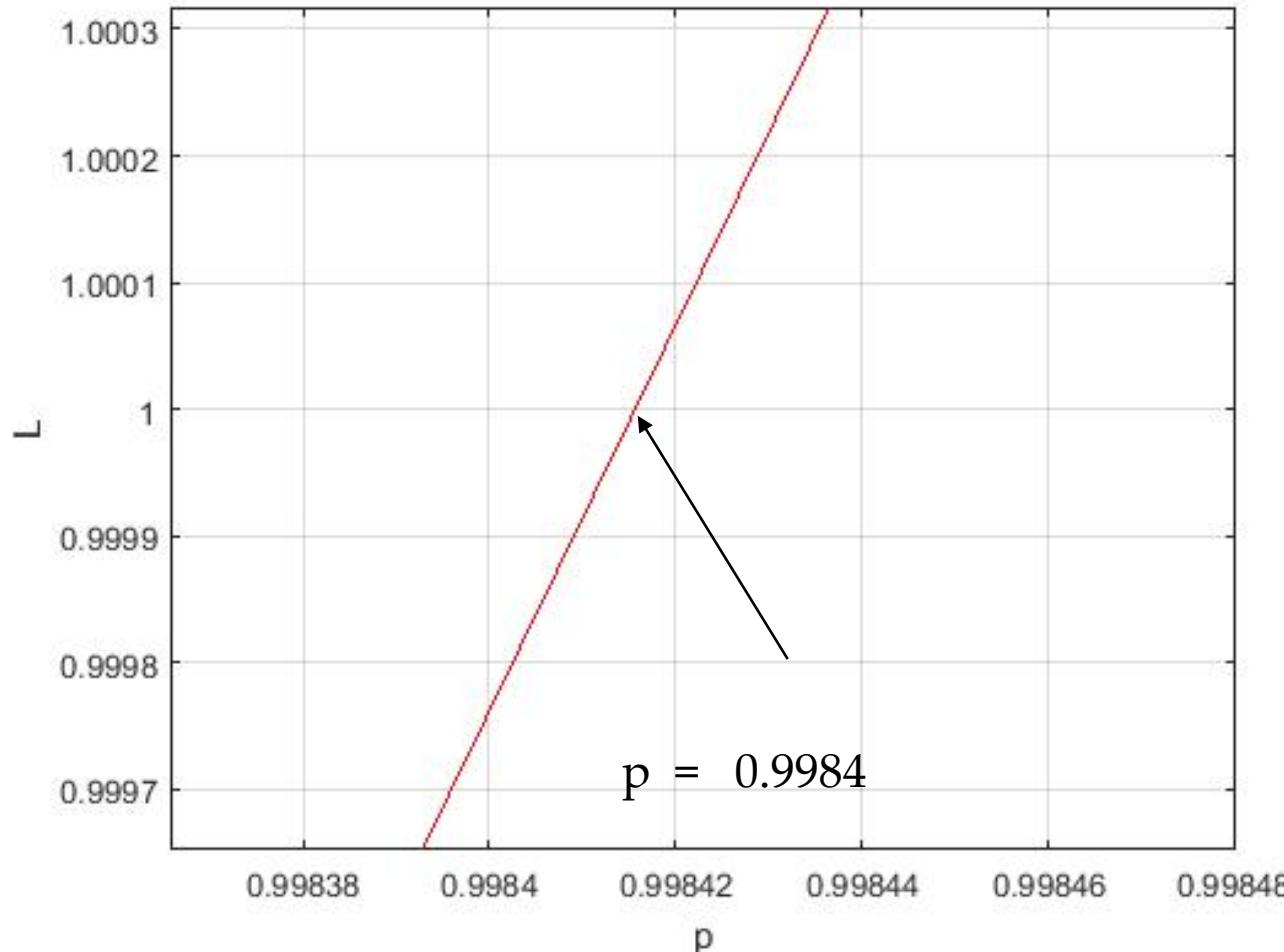
I =  $(5 \times 10^{-2})(1 \times 10^{-3})^3/12 \text{ m}^4$

$$\int_{\sin^{-1}\left(\frac{1}{p\sqrt{2}}\right)}^{\cos^{-1}\left(\frac{M}{2p}\sqrt{\frac{1}{FEI}}\right)} \frac{d\phi}{\sqrt{\frac{F}{EI}}\sqrt{1-p^2\sin^2\phi}} = L$$

# Finding $p$ with moment load equation



# Finding $p$ with moment load equation (close-up view)



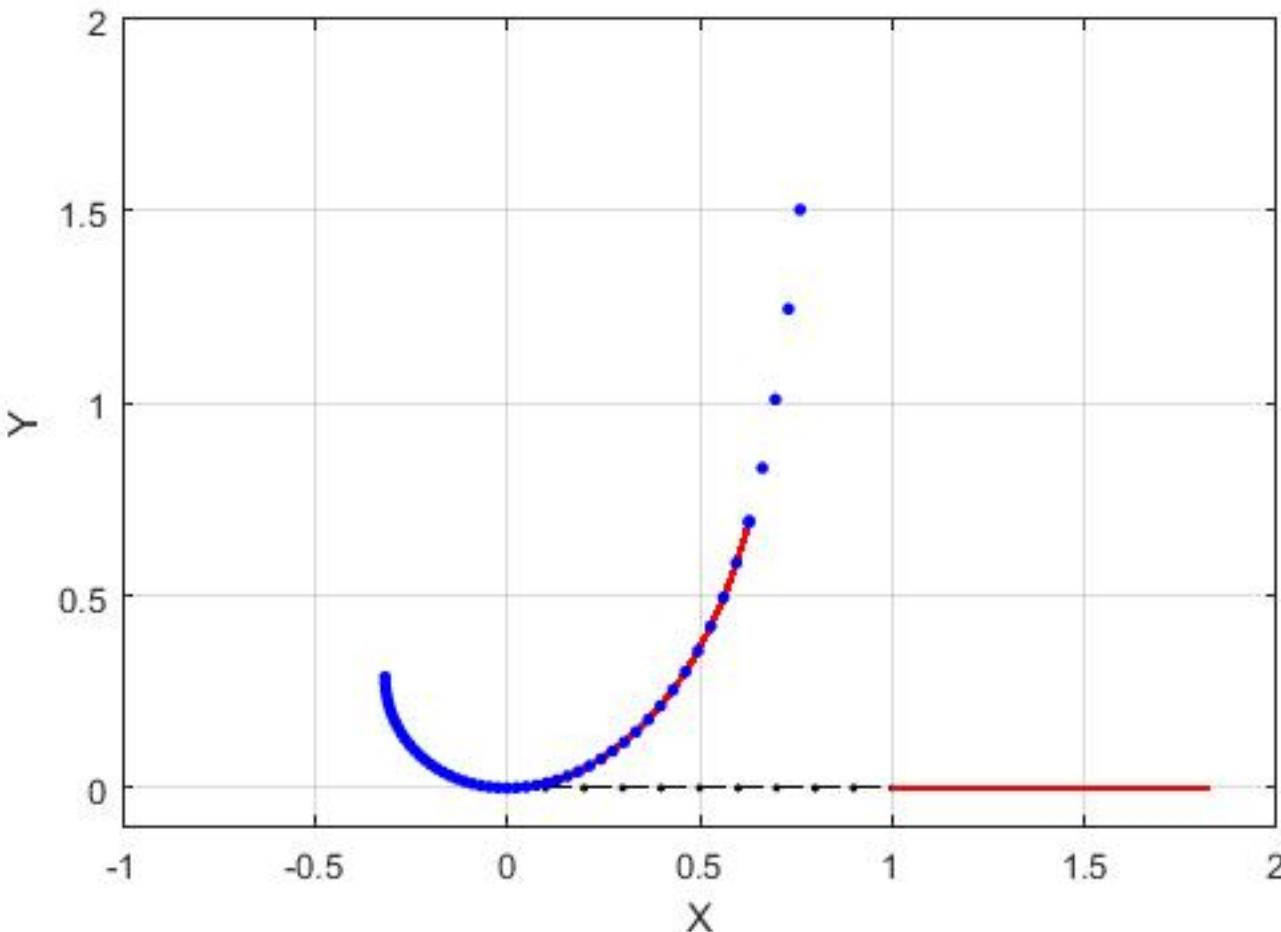
# Solution

$$e = M/F = 0.4/3 = 0.1333 \text{ m}$$

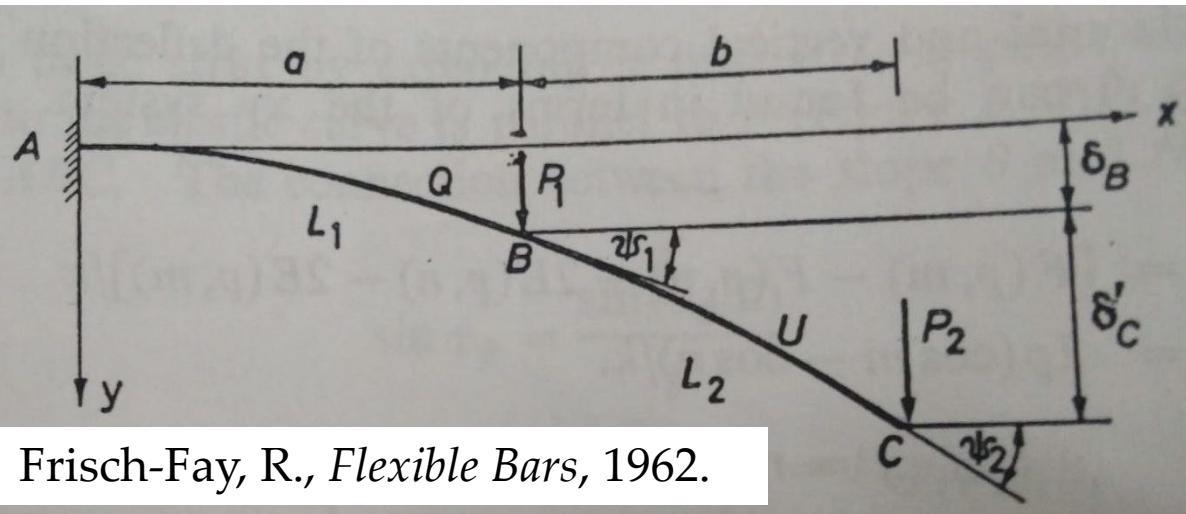
$$p = 0.9984$$

$$LM = \sqrt{EI/Fa} * (\text{ellipticF}(\pi/2, p^2) - \text{ellipticF}(\phi_1, p^2))$$

$$LM = 1.8257 \text{ m}$$



# Two transverse loads

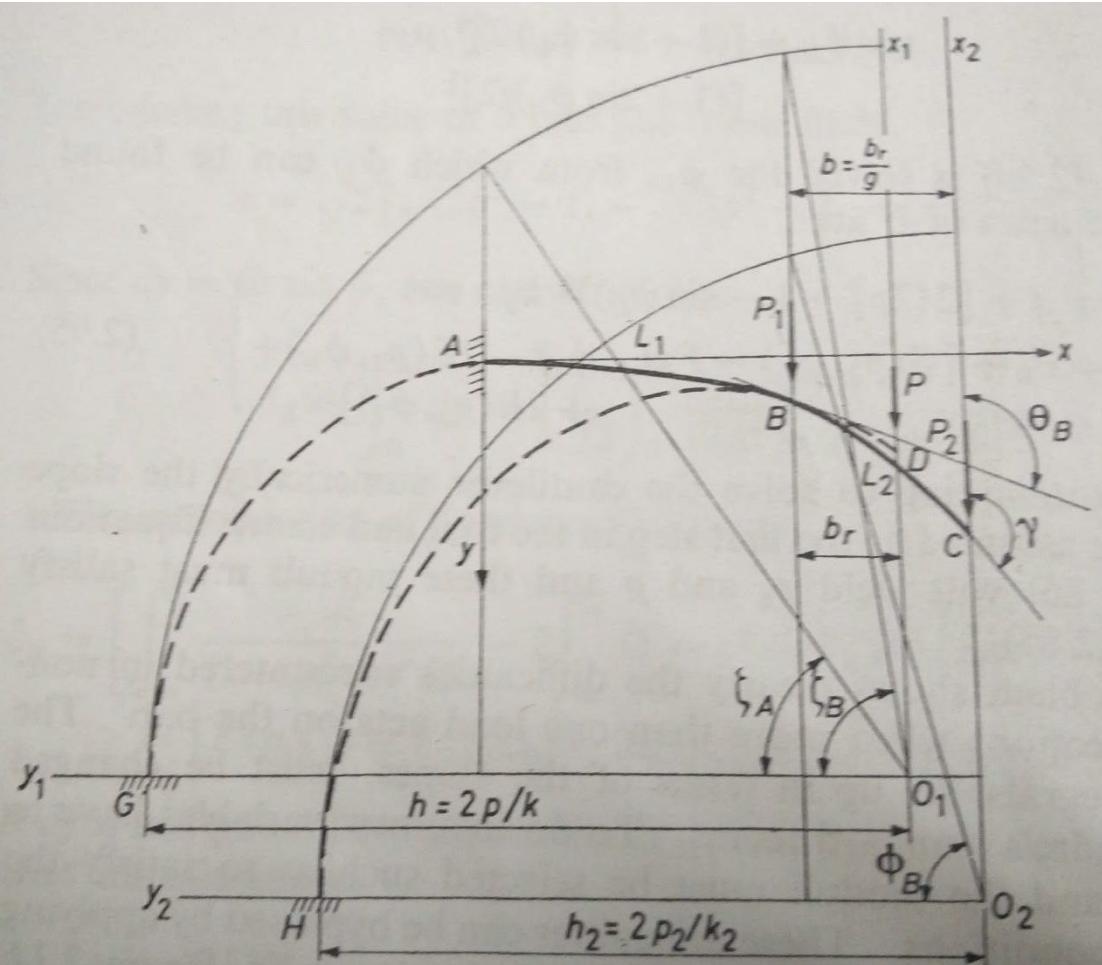


Frisch-Fay, R., *Flexible Bars*, 1962.

# Two transverse loads using elastic similarity

Frisch-Fay, R., *Flexible Bars*, 1962.

$$b = \frac{b_r}{g} \quad g = \frac{P_2}{P}$$



# What if there are $n$ loads?

- There will be as many  $p$ -unknowns as the number of loads.
- There will be as many  $\phi$ -unknowns as the number of loads less one.
- So,  $(2n-1)$  unknowns and as many equations in terms of elliptic integrals.

# Further reading

- Frisch-Fay, R., *Flexible Bars*, Butterworths, London, 1962.