

# Lecture 18b

## Size optimization of beams for stiffness and flexibility

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ME 260 at the Indian Institute of Science, Bengaluru

**Structural Optimization: Size, Shape, and Topology**

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# Outline of the lecture

Solving two problems concerning size optimization of beams for stiffness and flexibility with volume constraint.

What we will learn:

How to apply the eight steps we had used for bars to the case of beams.

# Problem 1

Minimize the mean compliance  
of a beam for given volume of  
material.

$$\underset{A(x)}{\text{Min}} \ MC = \int_0^L q w dx$$

Subject to

$$\lambda(x): \quad (EIw'')'' - q = 0 \Rightarrow (E\alpha Aw'')'' - q = 0$$

$$\Lambda: \quad \int_0^L A dx - V^* \leq 0$$

$$\text{Data: } L, q(x), E, \alpha = t^2/12, V^*$$



We assume here that only  $b(x)$  is variable.

$$I(x) = \alpha A^\beta$$
$$\alpha = \left( \frac{t^2}{12} \right); \beta = 1$$

# Steps in the solution procedure

Step 1: Write the Lagrangian

Step 2: Take variation of the Lagrangian w.r.t. the design variable and equate to zero to get the design equation.

Step 3: Take variation of the Lagrangian w.r.t. state variable(s) and equate to zero to get the adjoint equation(s).

Step 4: Collect all the equations, including the governing equation(s), complementarity condition(s), resource constraints, etc.

Step 5: Obtain the optimality criterion by substituting adjoint and equilibrium equations into the design equation, when it is possible.

Step 6: Identify all boundary conditions.

Step 7: Solve the equations analytically as much as possible.

Step 8: Use the optimality criteria method to solve the equations numerically.

# Solution

Minimize the mean compliance of a beam for given volume of material.

$$\underset{A(x)}{\text{Min}} \ MC = \int_0^L q w dx$$

Subject to

$$\lambda(x): \quad (EIw'')'' - q = 0 \Rightarrow (E\alpha Aw'')'' - q = 0$$

$$\Lambda: \quad \int_0^L A dx - V^* \leq 0$$

$$\text{Data: } L, q(x), E, \alpha = t^2/12, V^*$$

Step 1

$$L = \int_0^L \left\{ q w + \lambda \left( (E\alpha Aw'')'' - q \right) + \Lambda A \right\} dx - \Lambda V^*$$

# Expand the Lagrangian

Step 1

$$L = \int_0^L \left\{ q w + \lambda \left( (E\alpha A w'')'' - q \right) + \Lambda A \right\} dx - \Lambda V^*$$

$$L = \int_0^L \left\{ q w + \lambda \left( (E\alpha A w'')'' - q \right) + \Lambda A \right\} dx - \Lambda V^*$$

$$= \int_0^L \left\{ q w + E\alpha\lambda (A' w'' + A w''')' - \lambda q + \Lambda A \right\} dx - \Lambda V^*$$

$$= \int_0^L \left\{ q w + E\alpha\lambda A'' w'' + 2E\alpha\lambda A' w''' + E\alpha\lambda A w'''' - \lambda q + \Lambda A \right\} dx - \Lambda V^*$$

# Design equation

Step 2

$$L = \int_0^L \{qw + E\alpha\lambda A''w'' + 2E\alpha\lambda A'w''' + E\alpha\lambda Aw'''' - \lambda q + \Lambda A\} dx - \Lambda V^*$$

$$F = qw + E\alpha\lambda A''w'' + 2E\alpha\lambda A'w''' + E\alpha\lambda Aw'''' - \lambda q + \Lambda A$$

$$\delta_A L = 0 \Rightarrow \frac{\partial F}{\partial A} - \left( \frac{\partial F}{\partial A'} \right)' + \left( \frac{\partial F}{\partial A''} \right)'' = 0$$

$$\Rightarrow \Lambda + E\alpha\lambda w'''' - (2E\alpha\lambda w''')' + (E\alpha\lambda w'')'' = 0$$

$$\Rightarrow \Lambda + E\alpha\lambda w'''' - (2E\alpha\lambda w''')' + (E\alpha\lambda' w'')' + (E\alpha\lambda w''')' = 0$$

$$\Rightarrow \Lambda + E\alpha\lambda w'''' - (E\alpha\lambda w''')' + (E\alpha\lambda' w'')' = 0$$

$$\Rightarrow \Lambda + \textcolor{red}{E\alpha\lambda w''''} - (\textcolor{blue}{E\alpha\lambda' w'''}) - (\textcolor{red}{E\alpha\lambda w''''}) + (E\alpha\lambda'' w'') + (\textcolor{blue}{E\alpha\lambda' w'''}) = 0$$

$$\Rightarrow \Lambda + (E\alpha\lambda'' w'') = 0$$

# Adjoint equation

Step 3

$$F = qw + E\alpha\lambda A''w'' + 2E\alpha\lambda A'w''' + E\alpha\lambda Aw'''' - \lambda q + \Lambda A$$

$$\delta_w L = 0 \Rightarrow \frac{\partial F}{\partial w} - \left( \frac{\partial F}{\partial w'} \right)' + \left( \frac{\partial F}{\partial w''} \right)'' - \left( \frac{\partial F}{\partial w'''} \right)''' + \left( \frac{\partial F}{\partial w''''} \right)'''' = 0$$

$$\Rightarrow q - (0)' + (E\alpha\lambda A'')'' - (2E\alpha\lambda A')''' + (E\alpha\lambda A)'''' = 0$$

$$\Rightarrow q + (E\alpha\lambda A'')'' - (2E\alpha\lambda A')''' + (E\alpha\lambda' A)''' + (E\alpha\lambda A')''' = 0$$

$$\Rightarrow q + (E\alpha\lambda A'')'' - (E\alpha\lambda A')''' + (E\alpha\lambda' A)''' = 0$$

$$\Rightarrow q + (E\alpha\lambda A'')'' - (E\alpha\lambda' A')'' - (E\alpha\lambda A'')'' + (E\alpha\lambda'' A)'' + (E\alpha\lambda' A')'' = 0$$

$$\Rightarrow q + (E\alpha\lambda'' A)'' = 0$$

# Collect all equations

## Step 4

Unknowns  $A(x), w(x), \lambda(x), \Lambda$

Three functions and one scalar variable.

We have three differential equations and one scalar equation.

Design equation

$$\Lambda + (E\alpha\lambda''w'') = 0$$

Adjoint equation

$$q + (E\alpha\lambda''A)'' = 0$$

Governing equation

$$(E\alpha Aw'')'' - q = 0$$

$$\left. \begin{array}{l} \Lambda + (E\alpha\lambda''w'') = 0 \\ q + (E\alpha\lambda''A)'' = 0 \\ (E\alpha Aw'')'' - q = 0 \end{array} \right\} \lambda = -w$$

Feasibility condition

$$\int_0^L A dx - V^* \leq 0$$

## Step 5

$$E\alpha w''^2 = \Lambda$$

Strain energy density is uniform throughout the beam.

And,  $\Lambda$  cannot be zero.

So, the volume constraint is active.

Complementarity condition

$$\Lambda \left( \int_0^L A dx - V^* \right) = 0, \Lambda \geq 0$$

# Identify all boundary conditions

Step 6    Boundary conditions for  $A(x)$

$$F = qw + E\alpha\lambda A''w'' + 2E\alpha\lambda A'w''' + E\alpha\lambda Aw'''' - \lambda q + \Lambda A$$

$$\left( F_{A'} - (F_{A''})' \right) \delta A \Big|_0^L = 0 \quad \left. \left\{ 2E\alpha\lambda w''' - (E\alpha\lambda w'')' \right\} \delta A \right|_0^L = 0$$

and

$$\Rightarrow \left. \left\{ E\alpha\lambda w'''' - E\alpha\lambda' w'' \right\} \delta A \right|_0^L = 0$$

$$\underbrace{F_{A''} \delta A' \Big|_0^L = 0}_{\left. \left\{ E\alpha\lambda w'' \right\} \delta A' \right|_0^L = 0} \quad \Rightarrow \left. \left\{ -E\alpha w w''' + E\alpha w' w'' \right\} \delta A \right|_0^L = 0 \quad \text{since } \lambda = -w$$
$$\Rightarrow \left. \left\{ -E\alpha w w'' \right\} \delta A' \right|_0^L = 0 \Rightarrow \left. \left\{ E\alpha w w'' \right\} \delta A' \right|_0^L = 0$$

# Identify all boundary conditions

Step 6    Boundary conditions for  $\lambda(x)$

$$F = qw + E\alpha\lambda A''w'' + 2E\alpha\lambda A'w''' + E\alpha\lambda Aw'''' - \lambda q + \Lambda A$$

$$\left( F_{w'} - (F_{w''})' + (F_{w''''})'' - (F_{w''''''})''' \right) \delta w \Big|_0^L = 0$$

$$\left( F_{w''} - (F_{w''''})' + (F_{w''''''})'' \right) \delta w' \Big|_0^L = 0$$

$$\left( F_{w'''} - (F_{w''''})' \right) \delta w'' \Big|_0^L = 0$$

$$F_{w''''} \delta w''' \Big|_0^L = 0$$

# Identify all boundary conditions

Step 6    Boundary conditions for  $\lambda(x)$

$$F = qw + E\alpha\lambda A''w'' + 2E\alpha\lambda A'w''' + E\alpha\lambda Aw'''' - \lambda q + \Lambda A$$

$$\left( F_{w'} - (F_{w''})' + (F_{w''''})'' - (F_{w''''''})''' \right) \delta w \Big|_0^L = 0 \quad \left. \left( - (E\alpha\lambda A'')' + (2E\alpha\lambda A')'' - (E\alpha\lambda A)''' \right) \delta w \right|_0^L = 0$$

$$\left( F_{w''} - (F_{w''''})' + (F_{w''''''})'' \right) \delta w' \Big|_0^L = 0 \quad \left. \left\{ E\alpha\lambda A'' - (2E\alpha\lambda A')' + (E\alpha\lambda A)'' \right\} \delta w' \right|_0^L = 0$$

$$\left( F_{w''''} - (F_{w''''''})' \right) \delta w'' \Big|_0^L = 0 \quad \left. \left\{ 2E\alpha\lambda A' - (E\alpha\lambda A)' \right\} \delta w'' \right|_0^L = 0$$

$$\underbrace{F_{w''''} \delta w''' \Big|_0^L = 0}_{\text{Boundary condition}}$$

$$\left. (E\alpha\lambda A) \delta w''' \right|_0^L = 0$$

# Simplify 1<sup>st</sup> adjoint boundary condition

$$\left\{ -(E\alpha\lambda A'')' + (2E\alpha\lambda A')'' - (E\alpha\lambda A)''' \right\} \delta w \Big|_0^L = 0$$

$$\Rightarrow \left\{ -(E\alpha\lambda A'')' + (2E\alpha\lambda A')'' - (E\alpha\lambda A')'' - (E\alpha\lambda' A)'' \right\} \delta w \Big|_0^L = 0$$

$$\Rightarrow \left\{ -(E\alpha\lambda A'')' + (E\alpha\lambda A')'' - (E\alpha\lambda' A)'' \right\} \delta w \Big|_0^L = 0$$

$$\Rightarrow \left\{ -(E\alpha\lambda A'')' + (E\alpha\lambda A'')' + (E\alpha\lambda' A')' - (E\alpha\lambda' A)'' \right\} \delta w \Big|_0^L = 0$$

$$\Rightarrow \left\{ (E\alpha\lambda' A')' - (E\alpha\lambda' A)'' \right\} \delta w \Big|_0^L = 0 \Rightarrow \left\{ (E\alpha\lambda' A')' - (E\alpha\lambda' A')' - (E\alpha\lambda'' A)' \right\} \delta w \Big|_0^L = 0$$

$$\Rightarrow \left\{ -(E\alpha\lambda'' A)' \right\} \delta w \Big|_0^L = 0 \Rightarrow (E\alpha\lambda'' A' + E\alpha\lambda'' A) \delta w \Big|_0^L = 0$$

# Simplify 2<sup>nd</sup>-4<sup>th</sup> adjoint boundary conditions

$$\left\{ E\alpha\lambda A'' - (2E\alpha\lambda A')' + (E\alpha\lambda A)'' \right\} \delta w' \Big|_0^L = 0$$

$$\Rightarrow \left\{ E\alpha\lambda A'' - (2E\alpha\lambda A')' + (E\alpha\lambda A')' + (E\alpha\lambda' A)' \right\} \delta w' \Big|_0^L = 0$$

$$\Rightarrow \left\{ E\alpha\lambda A'' - (E\alpha\lambda A')' + (E\alpha\lambda' A)' \right\} \delta w' \Big|_0^L = 0$$

$$\Rightarrow \left\{ -(E\alpha\lambda' A') + (E\alpha\lambda' A)' \right\} \delta w' \Big|_0^L = 0 \Rightarrow (E\alpha\lambda'' A) \delta w' \Big|_0^L = 0$$

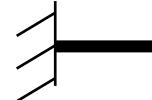
$$\left\{ 2E\alpha\lambda A' - (E\alpha\lambda A)' \right\} \delta w'' \Big|_0^L = 0 \Rightarrow (E\alpha\lambda A' - E\alpha\lambda' A) \delta w'' \Big|_0^L = 0$$

$$(E\alpha\lambda A) \delta w''' \Big|_0^L = 0$$

# All four adjoint boundary conditions

$$\delta w = \delta w' = 0$$

Fixed



$$\delta w = w'' = 0$$

Pinned



$$(E\alpha\lambda''A' + E\alpha\lambda'''A)\delta w|_0^L = 0$$

No BC for  $\lambda(x)$

No BC for  $\lambda(x)$

$$(E\alpha\lambda''A)\delta w'|_0^L = 0$$

No BC for  $\lambda(x)$

$$\lambda''A = 0$$

$$(E\alpha\lambda A' - E\alpha\lambda' A)\delta w''|_0^L = 0$$

$$\lambda A' - \lambda' A = 0$$

No BC for  $\lambda(x)$

$$(E\alpha\lambda A)\delta w'''|_0^L = 0$$

$$\lambda A = 0$$

$$\lambda A = 0$$

Notice that BCs of the state variable transfer to adjoint variable (most often).  
But be sure to keep the BCs on the design variable in mind.

# All four adjoint boundary conditions

$\delta w' = w''' = 0$	Transversely guided	$w'' = w''' = 0$
	Free	—

$$(E\alpha\lambda''A' + E\alpha\lambda'''A)\delta w|_0^L = 0 \quad \lambda''A' + \lambda'''A = 0 \quad \lambda''A' + \lambda'''A = 0$$


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$$(E\alpha\lambda''A)\delta w'|_0^L = 0 \quad \text{No BC for } \lambda(x) \quad \lambda''A = 0$$


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$$(E\alpha\lambda A' - E\alpha\lambda' A)\delta w''|_0^L = 0 \quad \lambda A' - \lambda' A = 0 \quad \text{No BC for } \lambda(x)$$


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$$(E\alpha\lambda A)\delta w'''|_0^L = 0 \quad \text{No BC for } \lambda(x) \quad \text{No BC for } \lambda(x)$$

Notice that BCs of the state variable transfer to adjoint variable (most often).  
But be sure to keep the BCs on the design variable in mind.

# Solving for a particular beam BCs

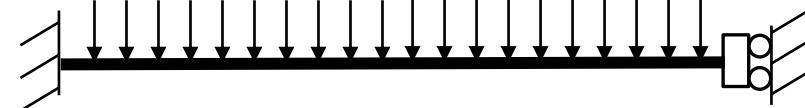
Step 7

Fixed

$q(x) = q_0$

Transversely  
guided

$$w = w' = 0$$



$$w' = w''' = 0$$

$$\lambda A = 0 \quad \& \quad \lambda A' - \lambda' A = 0$$

$$\text{Take } \lambda = \lambda' = 0$$

$$\{E\alpha w w''\} \delta A' \Big|_0^L = 0 \quad \& \quad \{-E\alpha w w''' + E\alpha w' w''\} \delta A \Big|_0^L = 0$$

Satisfied at  $x = 0$   
and  $x = L$

$$E\alpha w''^2 = \Lambda$$

$$\Rightarrow w'' = \pm \sqrt{\frac{\Lambda}{E\alpha}}$$

Satisfied at  $x = 0$   
and  $x = L$

$$\lambda'' A' + \lambda''' A = 0 \quad \& \quad \lambda A' - \lambda' A = 0$$

$$\text{Take } \lambda''' = \lambda' = A' = 0$$

$$C_1 = -\frac{q_0 L}{\sqrt{E\alpha\Lambda}}$$

$$\left( \pm A \sqrt{E\alpha\Lambda} \right)'' = q_0 \Rightarrow A = \pm \frac{q_0 x^2}{2\sqrt{E\alpha\Lambda}} + C_1 x + C_0$$

$$(E\alpha A w'')'' - q = 0$$

$$\text{Solve for } \Lambda \text{ using } \int_0^L A dx - V^* \leq 0$$

# Reconciliation of BCs for $A(x)$

Step 7

From the previous slide, we have  $A = \pm \frac{q_0 x^2}{2\sqrt{E\alpha\Lambda}} - \frac{q_0 L}{\sqrt{E\alpha\Lambda}} x + C_0$

We can use the active volume constraint to solve for  $\Lambda$

$$\Rightarrow \pm \frac{q_0 L^3}{6\sqrt{E\alpha\Lambda}} - \frac{q_0 L^3}{2\sqrt{E\alpha\Lambda}} + C_0 L = V^*$$

$$\Rightarrow \sqrt{E\alpha\Lambda} = -\frac{q_0 L^3}{3(V^* - C_0 L)} \quad \text{for + sign} \quad \& \quad \sqrt{E\alpha\Lambda} = -\frac{2q_0 L^3}{3(V^* - C_0 L)} \quad \text{for - sign}$$

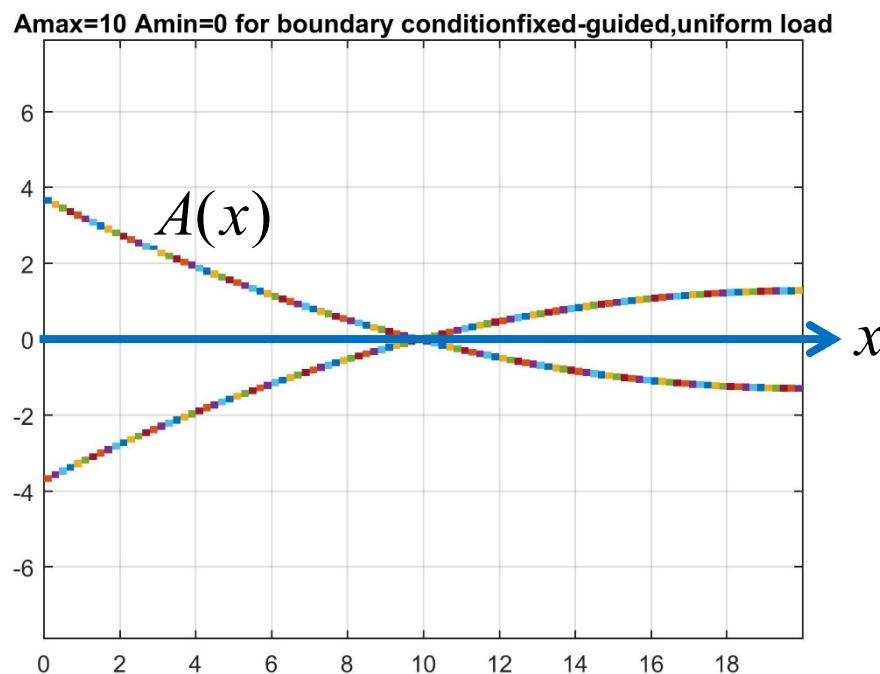
$$A(x) = \begin{cases} -\frac{3x^2(V^* - C_0 L)}{2L^3} - \frac{3(V^* - C_0 L)}{L^2} x + C_0 \\ \frac{3x^2(V^* - C_0 L)}{4L^3} - \frac{3(V^* - C_0 L)}{2L^2} x + C_0 \end{cases}$$

How do we choose the two possibilities (+ or -) and determine  $C_0$ ?

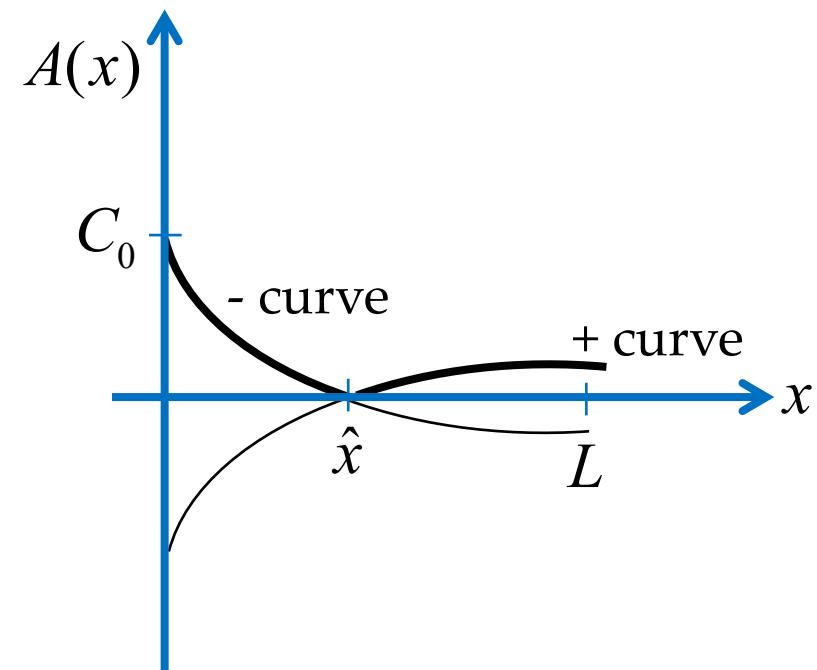
# Validating with the numerical solution...

$$A(x) = \begin{cases} A^+ = -\frac{3x^2(V^* - C_0L)}{2L^3} - \frac{3(V^* - C_0L)}{L^2}x + C_0 & + \text{curve} \\ A^- = \frac{3x^2(V^* - C_0L)}{4L^3} - \frac{3(V^* - C_0L)}{2L^2}x + C_0 & - \text{curve} \end{cases}$$

$$L = 20; d = 1; V^* = 50; E = 210; A_{\min} = 1E-3; A_{\max} = 10; q_0 = 1$$



We need to see which part of the domain should have the “+ curve” and which part should have “- curve”.



We need to find  $\hat{x}$  and  $C_0$  using  $A^+(\hat{x}) = A^-(\hat{x}) = 0$

# Problem 12

$$\underset{A(x)}{\text{Min}} V = \int_0^L A dx$$

Subject to

$$\lambda(x): (E\alpha Aw'')'' - q = 0$$

$$\lambda_d(x): (E\alpha Av'')'' - q_d = 0$$

$$\Lambda: \int_0^L E\alpha Aw''v'' dx - \Delta^* = 0$$

$$\Gamma: \int_0^L \frac{1}{2} E\alpha Aw''^2 dx - SE^* = 0$$

$$\text{Data: } L, q(x), q_d(x), \alpha = t^2/12, E, \Delta^*, SE^*$$

Minimize the volume of material of a beam (statically determinate or indeterminate) for a deflection constraint in its span with an upper bound on the strain energy.

# The end note

## Size optimization of beams

- We follow essentially the same eight steps
- Identifying the optimality criterion is the highlight.
- Boundary conditions for the adjoint variable need to be carefully done.  
See the correlation between BCs and optimal profiles
- Analytical solution may be segmented with multiple possibilities because of + and – of constant strain.
- Iterative numerical solution, when it is needed, remains the same.

Thanks